

# **OSCILLATORS**

# Objectives

- Describe the basic concept of an oscillator
- Discuss the basic principles of operation of an oscillator
- Describe the operation of Phase-Shift Oscillator, Wien Bridge Oscillator, Crystal Oscillator and Relaxation Oscillator

# Introduction

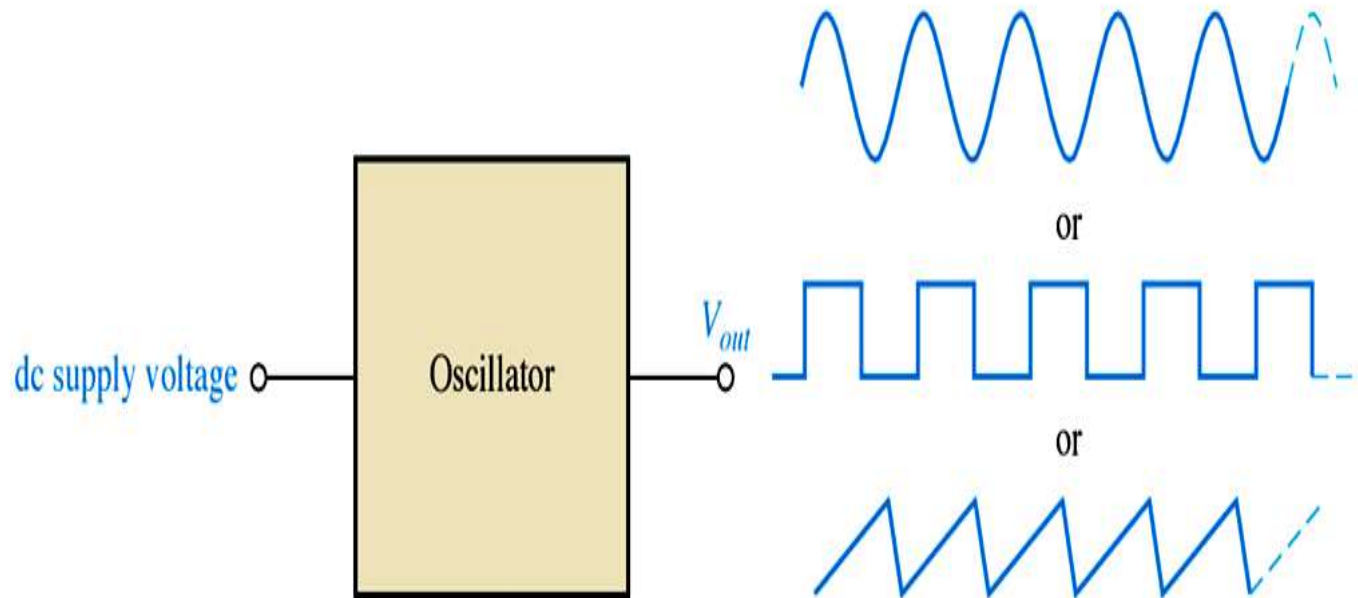
Oscillators are circuits that produce a continuous signal of some type without the need of an input.

These signals serve a variety of purposes such as communications systems, digital systems (including computers), and test equipment

# The Oscillator

- ❖ An oscillator is a circuit that produces a repetitive signal from a dc voltage.
- ❖ The **feedback oscillator** relies on a **positive feedback** of the output to maintain the oscillations.
- ❖ The **relaxation oscillator** makes use of an RC timing circuit to generate a non-sinusoidal signal such as square wave.

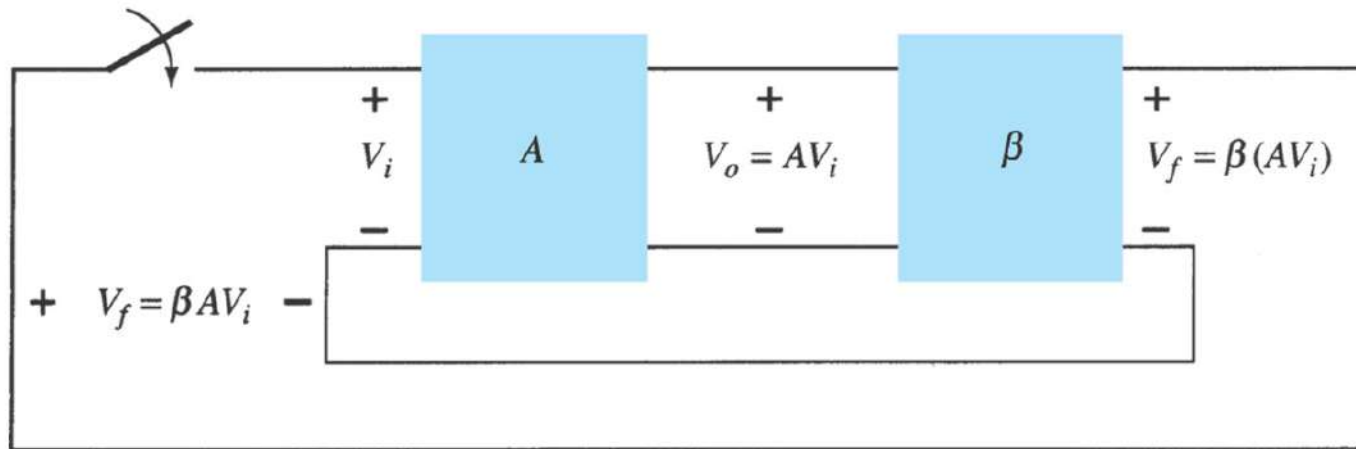
# The Oscillator



# Types of Oscillator

1. RC Oscillator - Wien Bridge Oscillator  
- Phase-Shift Oscillator
2. LC Oscillator - Crystal Oscillator
3. Relaxation Oscillator

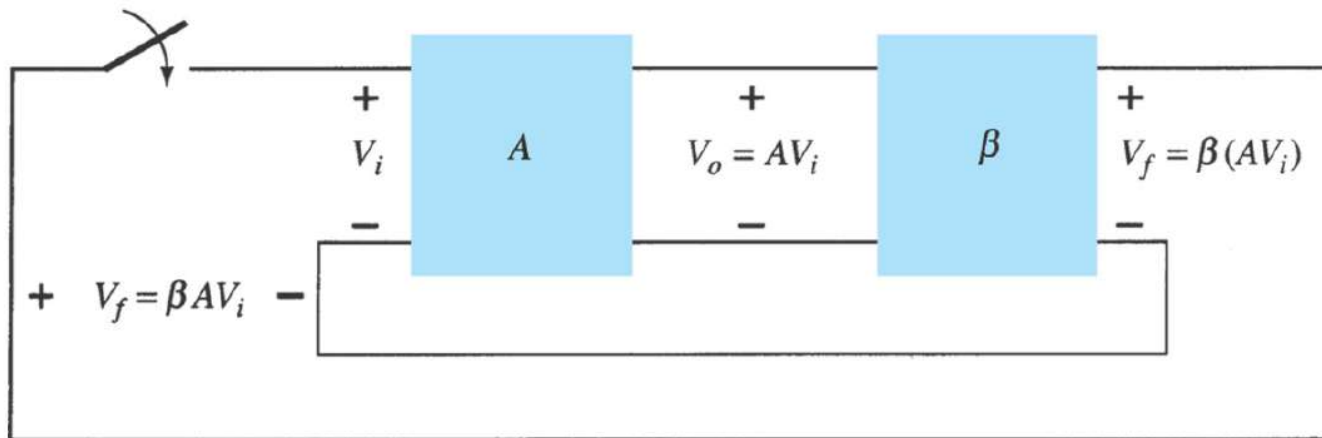
# Feedback Oscillator Principles



Positive feedback circuit used as an oscillator

- ❖ When switch at the amplifier input is open, no oscillation occurs.
- ❖ Consider  $V_i$ , results in  $V_o = AV_i$  (after amplifier stage) and  $V_f = \beta(AV_i)$  (after feedback stage)
- ❖ Feedback voltage  $V_f = \beta(AV_i)$  where  $\beta A$  is called the **loop gain**.
- ❖ In order to maintain  $V_f = V_i$ ,  $\beta A$  must be in the **correct magnitude** and **phase**.

# Feedback Oscillator Principles



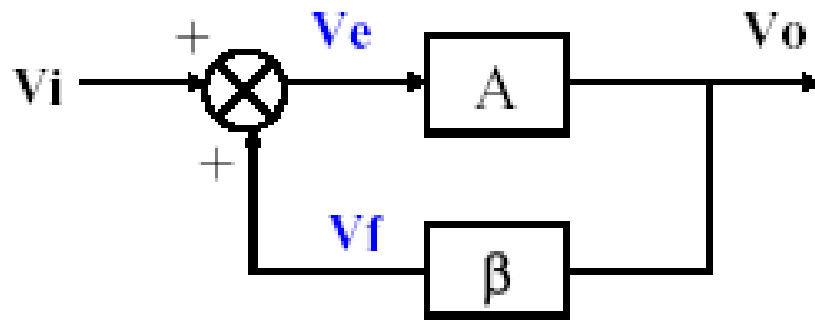
Positive feedback circuit used as an oscillator

- When the switch is closed and  **$V_i$  is removed**, the circuit **will continue operating** since the feedback voltage is sufficient to drive the amplifier and feedback circuit, resulting in proper input voltage to sustain the loop operation.



# Feedback Oscillator Principles

❖ An oscillator is an amplifier with **positive feedback**.



$$V_e = V_i + V_f \quad (1)$$

$$V_o = AV_e \quad (2)$$

$$V_f = \beta(AV_e) = \beta V_o \quad (3)$$

From (1), (2) and (3), we get

$$A_f \equiv \frac{V_o}{V_s} = \frac{A}{(1 - A\beta)}$$

where  $\beta A$  is **loop gain**

# Feedback Oscillator Principles

In general  $A$  and  $\beta$  are functions of frequency and thus may be written as;

$$A_f(s) = \frac{V_o}{V_s}(s) = \frac{A(s)}{1 - A(s)\beta(s)}$$

$A(s)\beta(s)$  is known as **loop gain**

## Feedback Oscillator Principles

Writing  $T(s) = A(s)\beta(s)$  the loop gain becomes;

$$A_f(s) = \frac{A(s)}{1 - T(s)}$$

Replacing  $s$  with  $j\omega$ ;

$$A_f(j\omega) = \frac{A(j\omega)}{1 - T(j\omega)}$$

and  $T(j\omega) = A(j\omega)\beta(j\omega)$

# Feedback Oscillator Principles

At a specific frequency  $f_0$ ;

$$T(j\omega_0) = A(j\omega_0)\beta(j\omega_0) = 1$$

At this frequency, the closed loop gain;

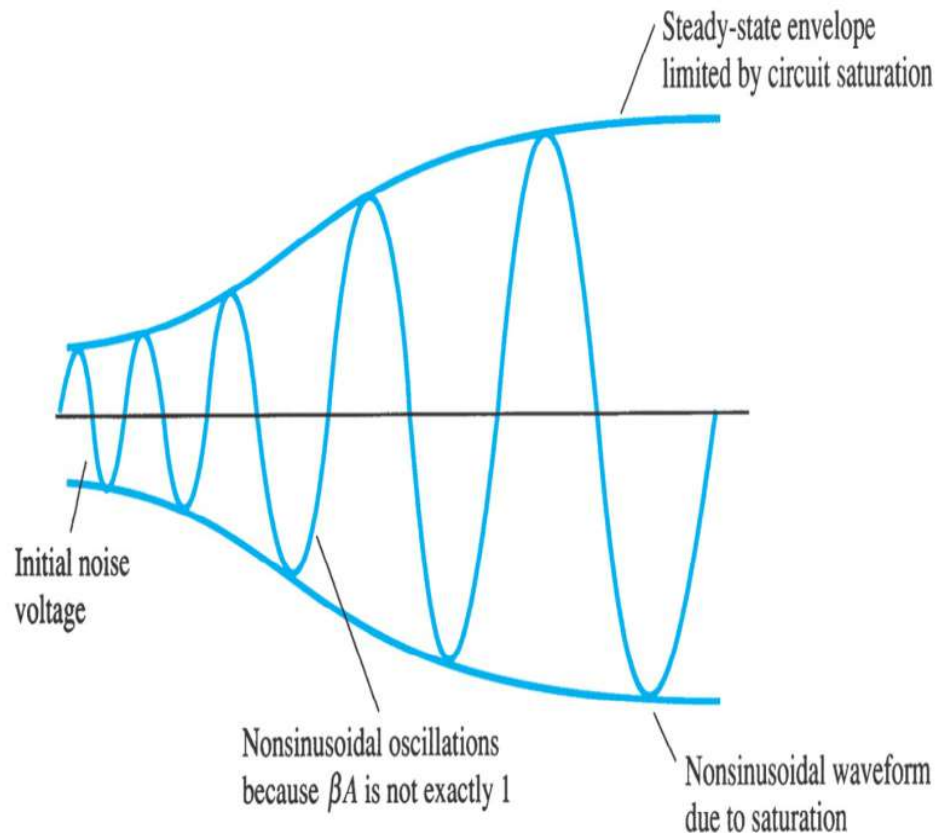
$$A_f(j\omega_0) = \frac{A(j\omega_0)}{1 - A(j\omega_0)\beta(j\omega_0)} = \frac{A(j\omega_0)}{(1-1)} = \infty$$

will be infinite, i.e. the circuit will have finite output for zero input signal – thus we have oscillation

# Design Criteria for oscillators

- 1)  $|A\beta|$  equal to **unity** or slightly larger at the desired oscillation frequency.  
- **Barkhausen criterion,  $|A\beta|=1$**
- 2) Total **phase shift,  $\phi$**  of the loop gain must be  **$0^\circ$**  or  **$360^\circ$** .

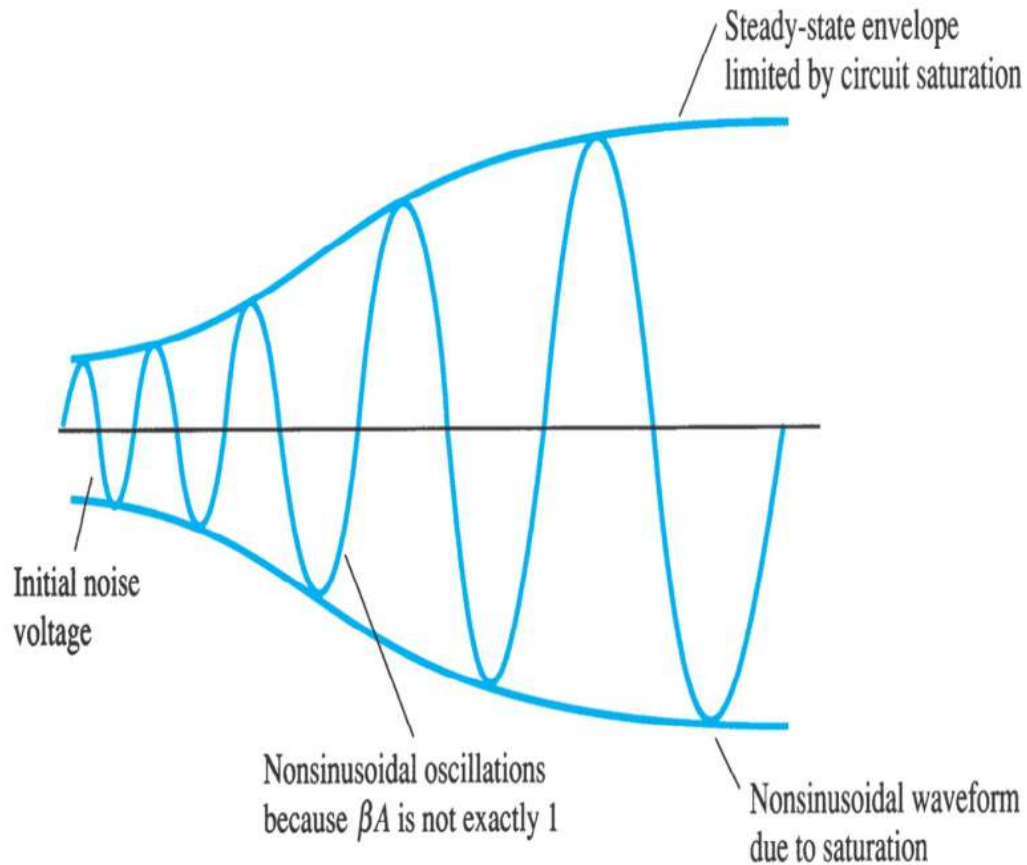
# Build-up of steady- state oscillations



Build-up of steady-state oscillations

- ❖ The unity gain condition must be met for oscillation to be sustained
- ❖ In practice, for oscillation to **begin**, the voltage gain around the positive feedback loop must be **greater than 1** so that the amplitude of the output can build up to the desired value.
- ❖ If the overall gain is greater than 1, the oscillator eventually saturates.

# Build-up of steady- state oscillations



❖ Then voltage gain decreases to 1 and maintains the desired amplitude of waveforms.

❖ The resulting waveforms are never exactly sinusoidal.

❖ However, the closer the value  $\beta A$  to 1, the more nearly sinusoidal is the waveform.

Buildup of steady-state oscillations

# Factors that determine the frequency of oscillation

- ❖ Oscillators can be classified into many types depending on the feedback components, amplifiers and circuit topologies used.
- ❖ RC components generate a sinusoidal waveform at a few Hz to kHz range.
- ❖ LC components generate a sine wave at frequencies of 100 kHz to 100 MHz.
- ❖ Crystals generate a square or sine wave over a wide range, i.e. about 10 kHz to 30 MHz.



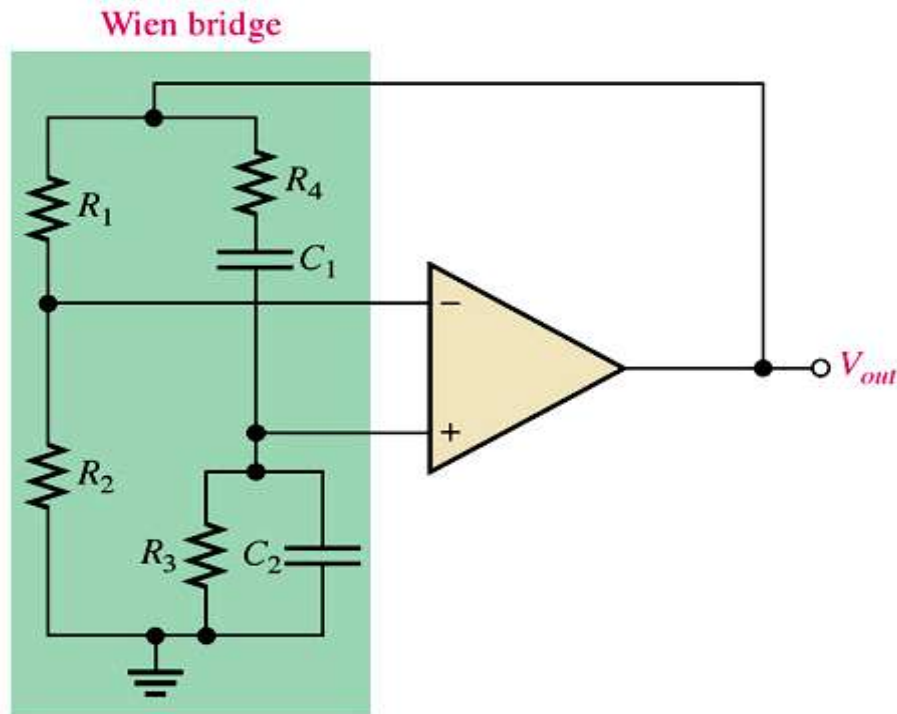
# 1. RC Oscillators

## 1. RC Oscillators

- ❖ RC feedback oscillators are generally limited to frequencies of 1MHz or less
- ❖ The types of RC oscillators that we will discuss are the Wien-Bridge and the Phase Shift

# Wien-Bridge Oscillator

- It is a low frequency oscillator which ranges from a few kHz to 1 MHz.
- Structure of this oscillator is



# Wien-Bridge Oscillator

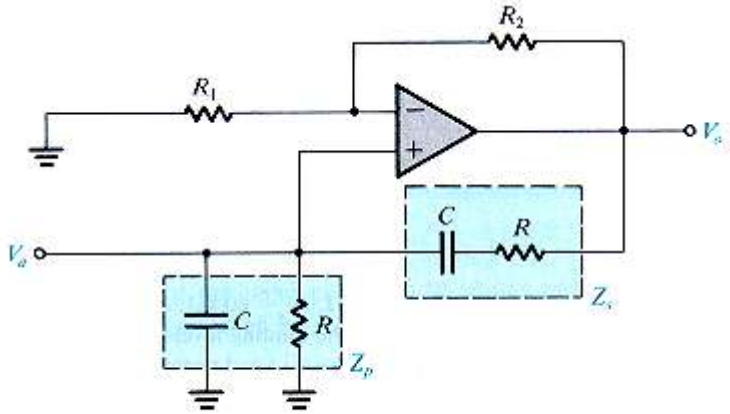
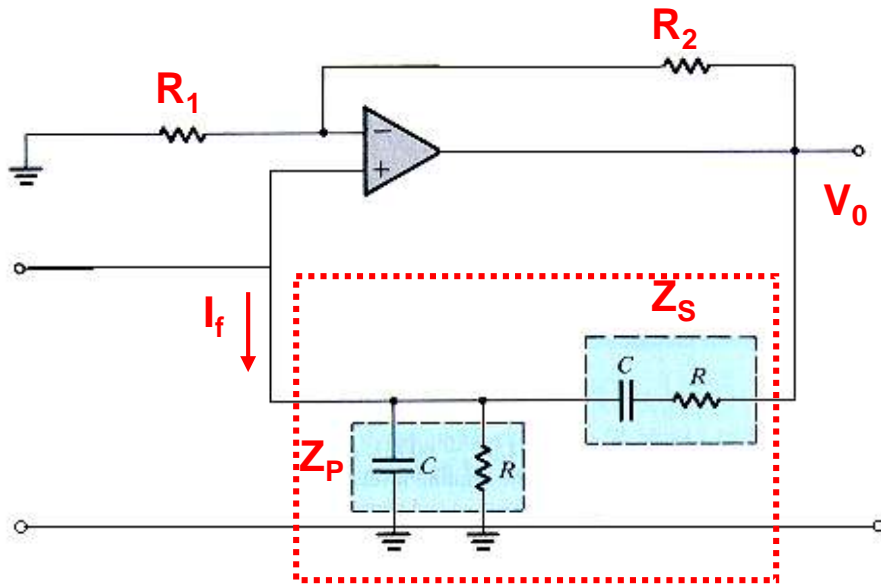
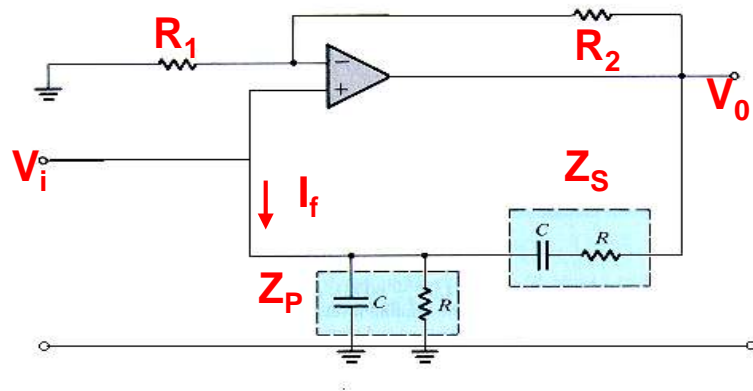


Fig. 12.4 Wien-bridge oscillator without amplitude stabilization.

- Based on op amp
- Combination of R's and C's in feedback loop so feedback factor  $\beta_f$  has a **frequency dependence**.
- Analysis assumes op amp is ideal.
  - Gain A is very large
  - Input currents are negligibly small ( $I_+ \approx I_- \approx 0$ ).
  - Input terminals are virtually shorted ( $V_+ \approx V_-$ ).
- Analyze like a normal feedback amplifier.
  - Determine input and output loading.
  - Determine feedback factor.
  - Determine gain with feedback.
- **Shunt-shunt** configuration.



# Wien Bridge Oscillator



**Define**

$$Z_S = R + Z_C = R + \frac{1}{sC} = \frac{1 + sRC}{sC}$$

$$Z_P = R \parallel Z_C = \left( \frac{1}{R} + \frac{1}{Z_C} \right)^{-1} = \left( \frac{1}{R} + sC \right)^{-1}$$
$$= \frac{R}{1 + sCR}$$

# Wien-Bridge Oscillator

## Oscillation condition

Phase of  $\beta_f A_r$  equal to  $180^\circ$ . It already is since  $\beta_f A_r < 0$ .

$$\text{Then need only } |\beta_f A_r| = \left(1 + \frac{R_2}{R_1}\right) \frac{sCR}{sCR + (1 + sCR)^2} = 1$$

Rewriting

$$\begin{aligned} |\beta_f A_r| &= \left(1 + \frac{R_2}{R_1}\right) \frac{sCR}{sCR + (1 + sCR)^2} \\ &= \left(1 + \frac{R_2}{R_1}\right) \frac{sCR}{sCR + (1 + 2sCR + s^2 C^2 R^2)} \\ &= \left(1 + \frac{R_2}{R_1}\right) \frac{sCR}{1 + 3sCR + s^2 C^2 R^2} = \left(1 + \frac{R_2}{R_1}\right) \frac{1}{3 + \frac{1}{sCR} + sCR} \\ &= \left(1 + \frac{R_2}{R_1}\right) \frac{1}{3 + j\left(\omega CR - \frac{1}{\omega CR}\right)} \end{aligned}$$

Then imaginary term = 0 at the oscillation frequency

$$\omega = \omega_o = \frac{1}{RC}$$

Then, we can get  $|\beta_f A_r| = 1$  by selecting the resistors  $R_1$  and  $R_2$  appropriately using

$$\left(1 + \frac{R_2}{R_1}\right) \frac{1}{3} = 1 \quad \text{or} \quad \frac{R_2}{R_1} = 2$$

# Wien-Bridge Oscillator

Multiply the top and bottom by  $j\omega C_1$ , we get

$$\frac{V_1}{V_o} = \frac{j\omega C_1 R_2}{(1 + j\omega C_1 R_1)(1 + j\omega C_2 R_2) + j\omega C_1 R_2}$$

Divide the top and bottom by  $C_1 R_1 C_2 R_2$

$$\frac{V_1}{V_o} = \frac{j\omega}{R_1 C_2 \left( \frac{1}{R_1 C_1 R_2 C_2} + j\omega \left( \frac{R_1 C_1 + R_2 C_2 + R_2 C_1}{R_1 C_1 R_2 C_2} \right) - \omega^2 \right)}$$

# Wien-Bridge Oscillator

Now the amp gives

$$\frac{V_0}{V_1'} = K$$

Furthermore, for steady state oscillations, we want the feedback  $V_1$  to be exactly equal to the amplifier input,  $V_1'$ . Thus

$$\frac{V_1'}{V_o} = \frac{1}{K} = \frac{V_1}{V_o}$$



# Wien-Bridge Oscillator

Hence

$$\frac{1}{K} = \frac{j\omega}{R_1 C_2 \left( \frac{1}{R_1 C_1 R_2 C_2} + j\omega \left( \frac{R_1 C_1 + R_2 C_2 + R_2 C_1}{R_1 C_1 R_2 C_2} \right) - \omega^2 \right)}$$

$$\frac{j\omega K}{R_1 C_2} = \left( \frac{1}{R_1 C_1 R_2 C_2} + j\omega \left( \frac{R_1 C_1 + R_2 C_2 + R_2 C_1}{R_1 C_1 R_2 C_2} \right) - \omega^2 \right)$$

Equating the real parts,

$$\frac{1}{R_1 C_1 R_2 C_2} - \omega^2 = 0$$

$$K = \frac{R_1 C_1 + R_2 C_2 + R_2 C_1}{R_2 C_1}$$

# Wien-Bridge Oscillator

If  $R_1 = R_2 = R$  and  $C_1 = C_2 = C$

$$K = 3$$



$A_{cl}$

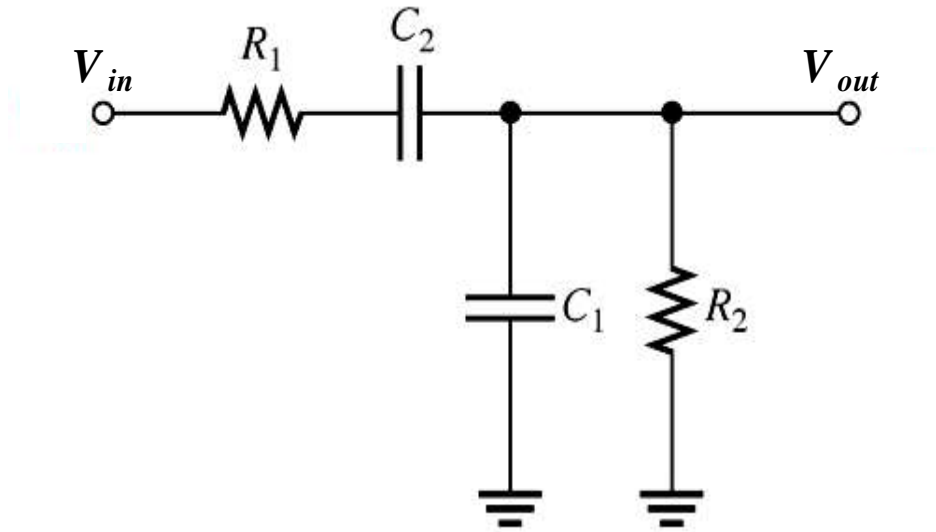
$$\omega = \frac{1}{RC}$$

$$f_r = \frac{1}{2\pi RC}$$

- Gain  $> 3$  : growing oscillations
- Gain  $< 3$  : decreasing oscillations

$K = 3$  ensured the loop gain of unity - oscillation

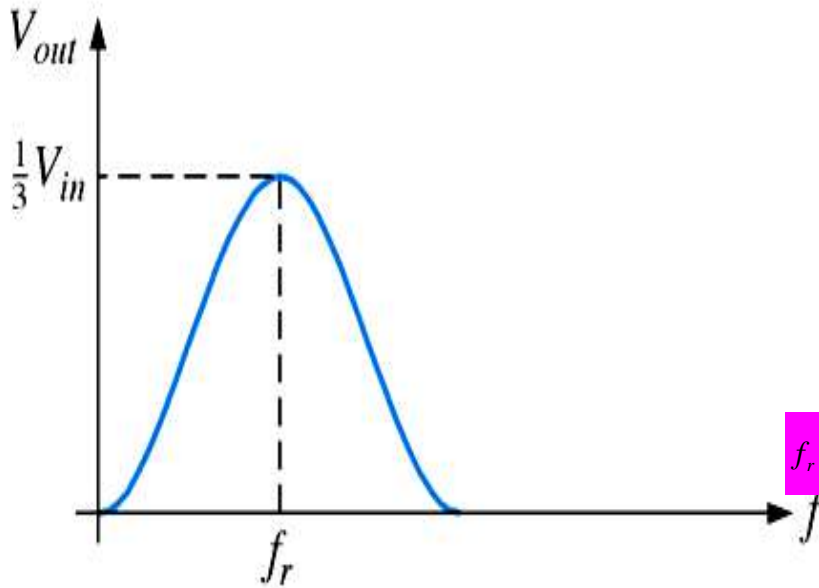
# Wien-Bridge Oscillator



A lead-lag circuit

- ❖ The fundamental part of the Wien-Bridge oscillator is a lead-lag circuit.
- ❖ It is comprised of  $R_1$  and  $C_1$  is the *lag* portion of the circuit,  $R_2$  and  $C_2$  form the *lead* portion

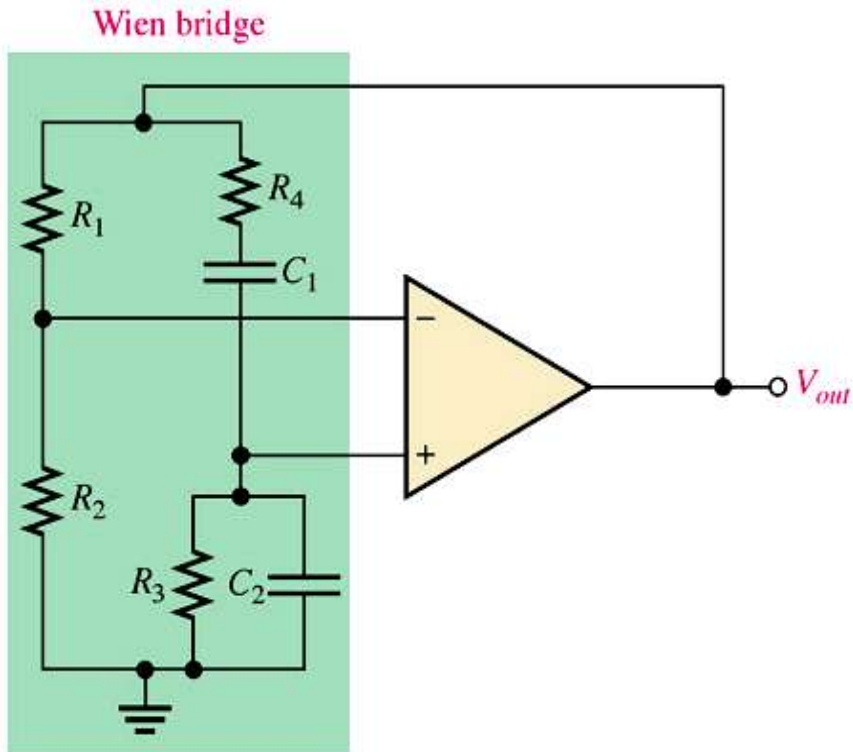
# Wien-Bridge Oscillator



Response Curve

- ❖ The lead-lag circuit of a Wien-bridge oscillator **reduces** the input signal by 1/3 and yields a response curve as shown.
- ❖ The response curve indicates that the output voltage peaks at a frequency is called **frequency resonant**.
- ❖ The frequency of resonance can be determined by the formula below.

# Wien-Bridge Oscillator

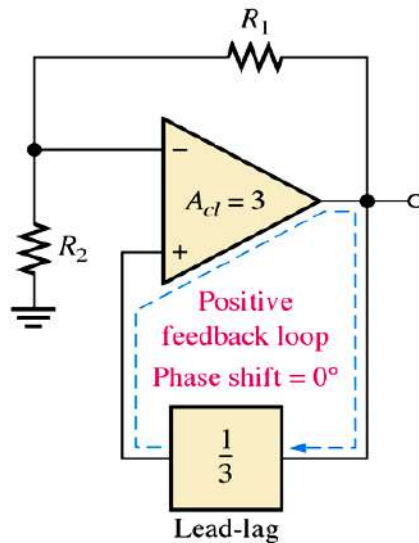


(b) Wien bridge circuit combines a voltage divider and a lead-lag circuit.

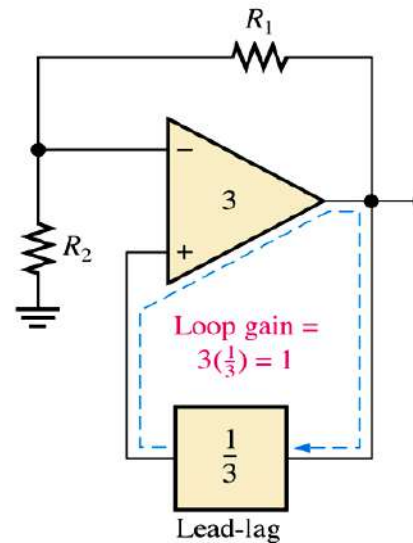
Basic circuit

- ❖ The lead-lag circuit is in the positive feedback loop of Wien-bridge oscillator.
- ❖ The **voltage divider limits gain (determines the closed-loop gain)**. The lead lag circuit is basically a band-pass with a narrow bandwidth.
- ❖ The Wien-bridge oscillator circuit can be viewed as a noninverting amplifier configuration with the input signal fed back from the output through the lead-lag circuit.

# Wien-Bridge Oscillator



(a) The phase shift around the loop is  $0^\circ$ .



(b) The voltage gain around the loop is 1.

## Conditions for sustained oscillation

- ❖ The  $0^\circ$  phase-shift condition is met when the frequency is  $f_r$  because the phase-shift through the lead lag circuit is  $0^\circ$
- ❖ The unity gain condition in the feedback loop is met when  $A_{cl} = 3$

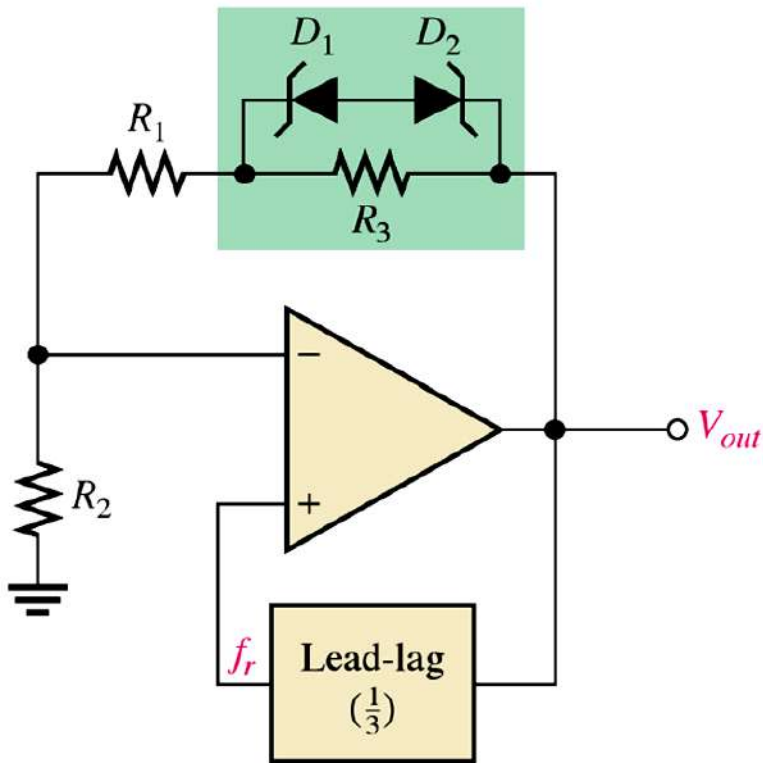
# Wien-Bridge Oscillator

- ❖ Since there is a loss of about 1/3 of the signal in the positive feedback loop, the **voltage-divider ratio** must be adjusted such that a positive feedback loop gain of **1** is produced.
- ❖ This requires a closed-loop gain of 3.
- ❖ The ratio of  $R_1$  and  $R_2$  can be set to achieve this. In order to achieve a closed loop gain of 3,  $R_1 = 2R_2$

$$\frac{R_1}{R_2} = 2$$

To ensure oscillation, the ratio  $R_1/R_2$  must be slightly greater than 2.

# Wien-Bridge Oscillator



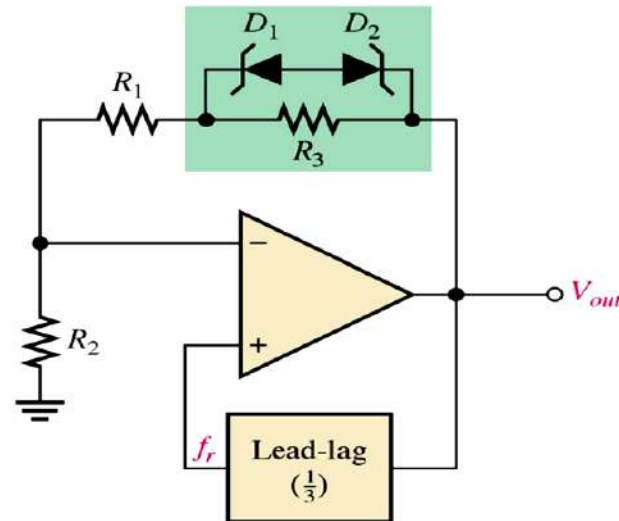
- ❖ To start the oscillations an initial gain greater than 1 must be achieved.
- ❖ The back-to-back zener diode arrangement is one way of achieving this with additional resistor  $R_3$  in parallel.
- ❖ When dc is first applied the zeners appear as opens. This places  $R_3$  in series with  $R_1$ , thus increasing the closed loop gain of the amplifier.

Self-starting Wien-bridge oscillator using back-to-back Zener diodes

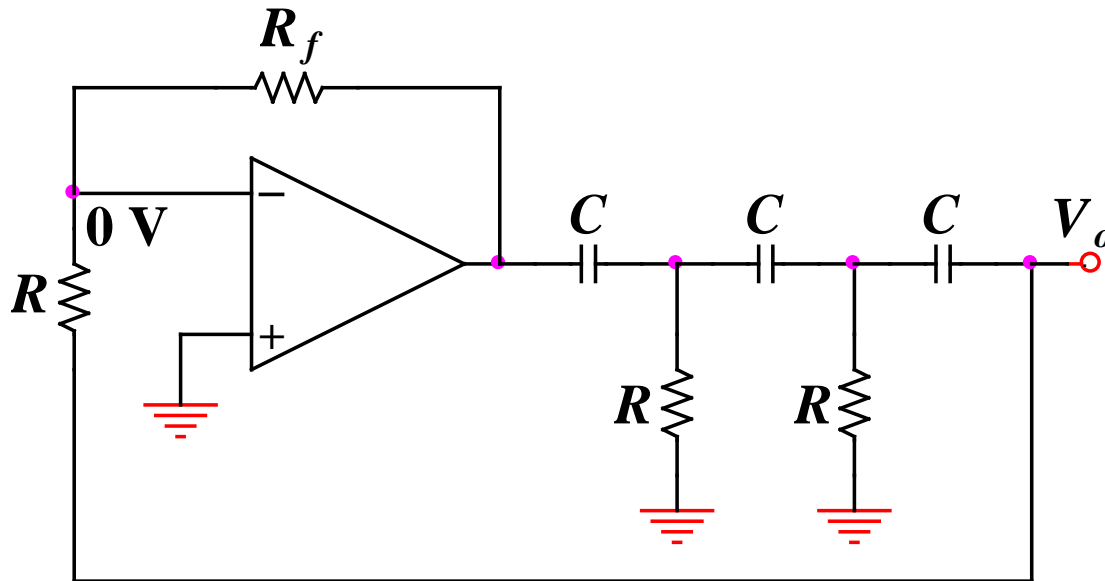


# Wien-Bridge Oscillator

- ❖ The lead-lag circuit permits only a signal with a frequency equal to  $f_r$  to appear in phase on the noninverting input. The feedback signal is amplified and continually reinforced, resulting in a buildup of the output voltage.
- ❖ When the output signal reaches the zener breakdown voltage, the zener conducts and shorts  $R_3$ . The amplifier's closed loop gain lowers to 3. At this point, the total loop gain is 1 and the oscillation is sustained.



# Phase-Shift Oscillator



Phase-shift oscillator

- ❖ The phase shift oscillator utilizes **three RC circuits** to provide  $180^\circ$  phase shift that when coupled with the  $180^\circ$  of the op-amp itself provides the necessary feedback to sustain oscillations.

- ❖ The frequency for this type is similar to any RC circuit oscillator :

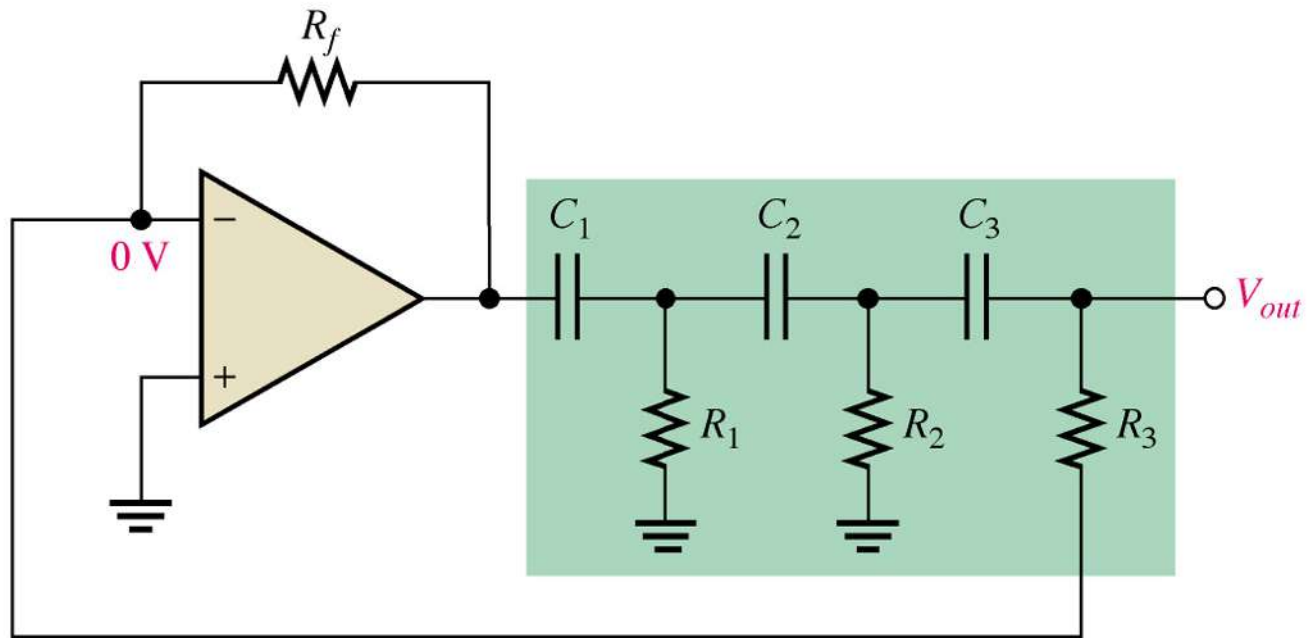
$$f = \frac{1}{2\pi RC\sqrt{6}}$$

where  $\beta = 1/29$  and the phase-shift is  $180^\circ$

- ❖ For the loop gain  $\beta A$  to be greater than unity, the gain of the amplifier stage must be greater than 29.
- ❖ If we measure the phase-shift per RC section, each section would not provide the same phase shift (although the overall phase shift is  $180^\circ$ ).
- ❖ In order to obtain exactly  $60^\circ$  phase shift for each of three stages, emitter follower stages would be needed for each RC section.

The gain must be at least 29 to maintain the oscillation

# Phase-Shift Oscillator



The transfer function of the RC network is

$$\mathbf{TF} = \frac{\mathbf{V_{in}}}{\mathbf{V_o}} = \frac{\mathbf{1}}{(\mathbf{SRC})^3 + \mathbf{5(SRC)^2} + \mathbf{6(SRC)} + \mathbf{1}}$$

# Phase-Shift Oscillator

If the gain around the loop equals 1, the circuit oscillates at this frequency. Thus for the oscillations we want,

$$\mathbf{K ( TF ) = 1}$$

$$\mathbf{or (SRC)^3 + 5(SRC)^2 + 6(SRC) + 1 - K = 0}$$

Putting  $s=j\omega$  and equating the real parts and imaginary parts, we obtain

$$-j\omega^3 (RC)^3 + 6j\omega RC = 0 \dots (1) \quad \mathbf{(Imaginary Part)}$$

$$-5\omega^2 (RC)^2 + 1 - K = 0 \dots (2) \quad \mathbf{(Real Part)}$$

# Phase-Shift Oscillator

From equation (1) ;

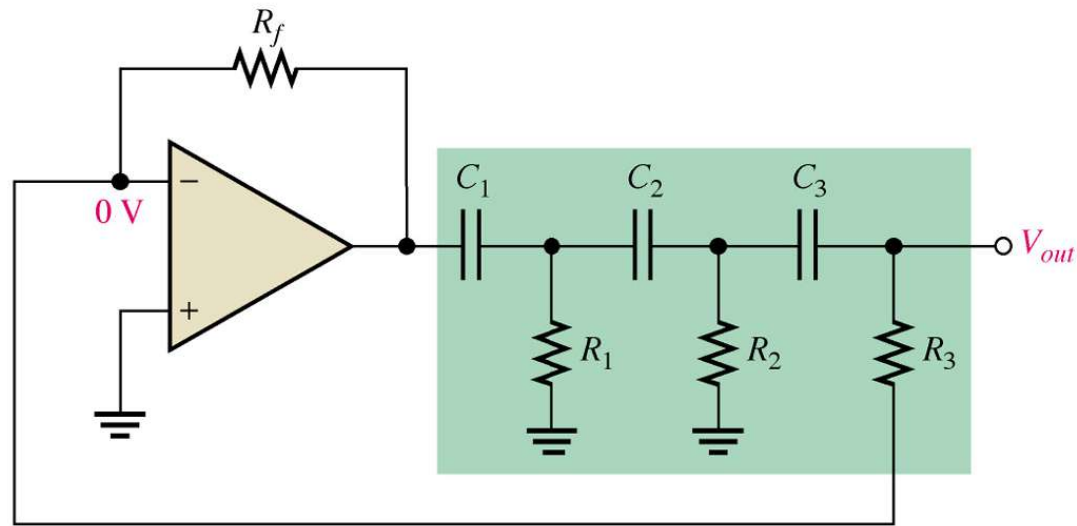
$$-\omega^2 (\mathbf{RC})^2 + 6 = 0$$
$$\omega = \frac{\sqrt{6}}{(\mathbf{RC})}$$

Substituting into equation (2) ;

$$-5 \left[ \frac{6}{(\mathbf{RC})^2} \right] (\mathbf{RC})^2 + 1 = \mathbf{K}$$
$$\Rightarrow \mathbf{K} = -29$$

# The gain must be at least 29 to maintain the oscillations.

# Phase Shift Oscillator – Practical



The last R has been incorporated into the summing resistors at the input of the inverting op-amp.

$$f_r = \frac{1}{2\pi\sqrt{6RC}}$$

$$K = \frac{-R_f}{R_3} = -29$$

## 2. LC Oscillators



# Oscillators With LC Feedback Circuits

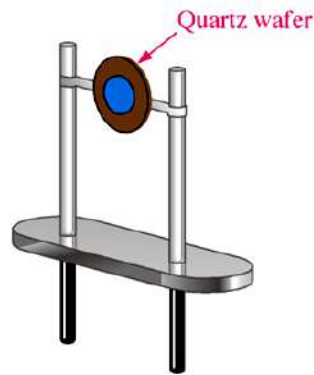
- ❖ For frequencies above 1 MHz, LC feedback oscillators are used.
- ❖ We will discuss the **crystal-controlled** oscillators.
- ❖ Transistors are used as the active device in these types.

# Crystal Oscillator

The crystal-controlled oscillator is the most stable and accurate of all oscillators. A crystal has a natural frequency of resonance. Quartz material can be cut or shaped to have a certain frequency. We can better understand the use of a crystal in the operation of an oscillator by viewing its electrical equivalent.



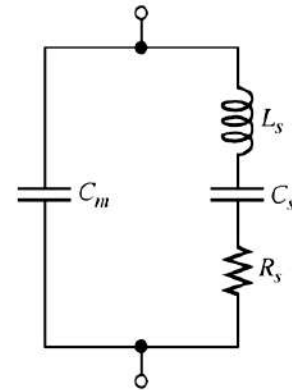
(a) Typical packaged crystal



(b) Basic construction (without case)



(c) Symbol



(d) Electrical equivalent

# Crystal Oscillator

The crystal appears as a resonant circuit (tuned circuit oscillator).

The crystal has two resonant frequencies:

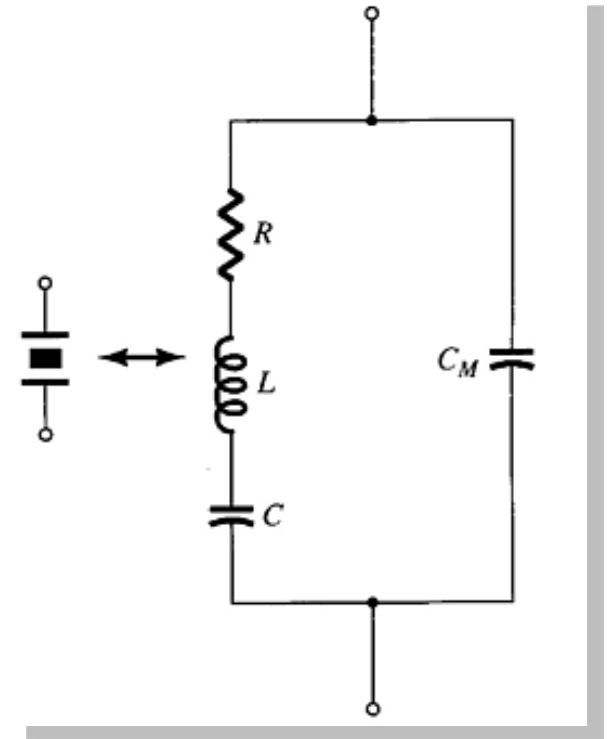
## Series resonant condition

- RLC determine the resonant frequency
- The crystal has a low impedance

## Parallel resonant condition

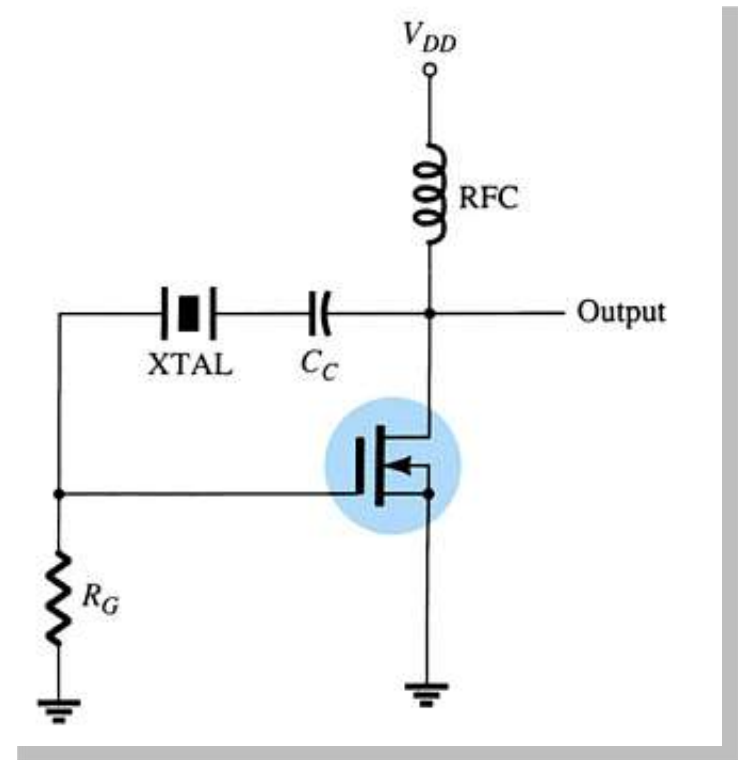
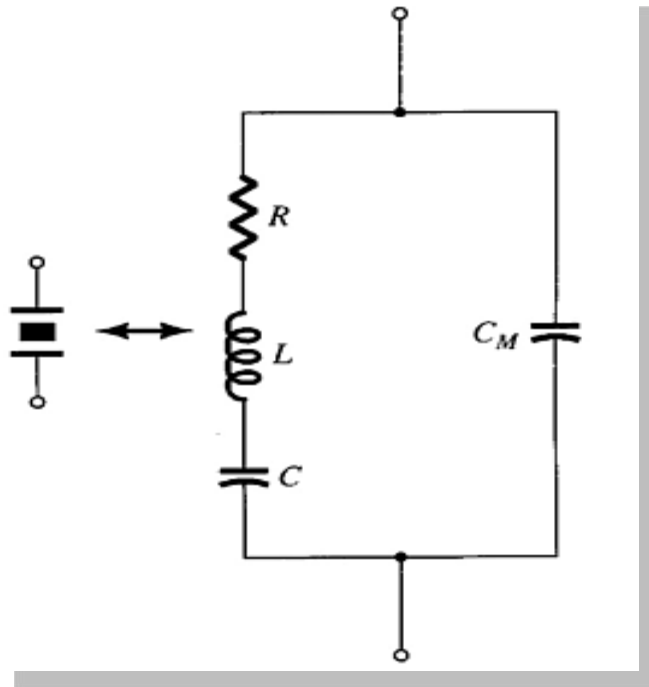
- RLC and  $C_M$  determine the resonant frequency
- The crystal has a high impedance

The series and parallel resonant frequencies are very close, within 1% of each other.



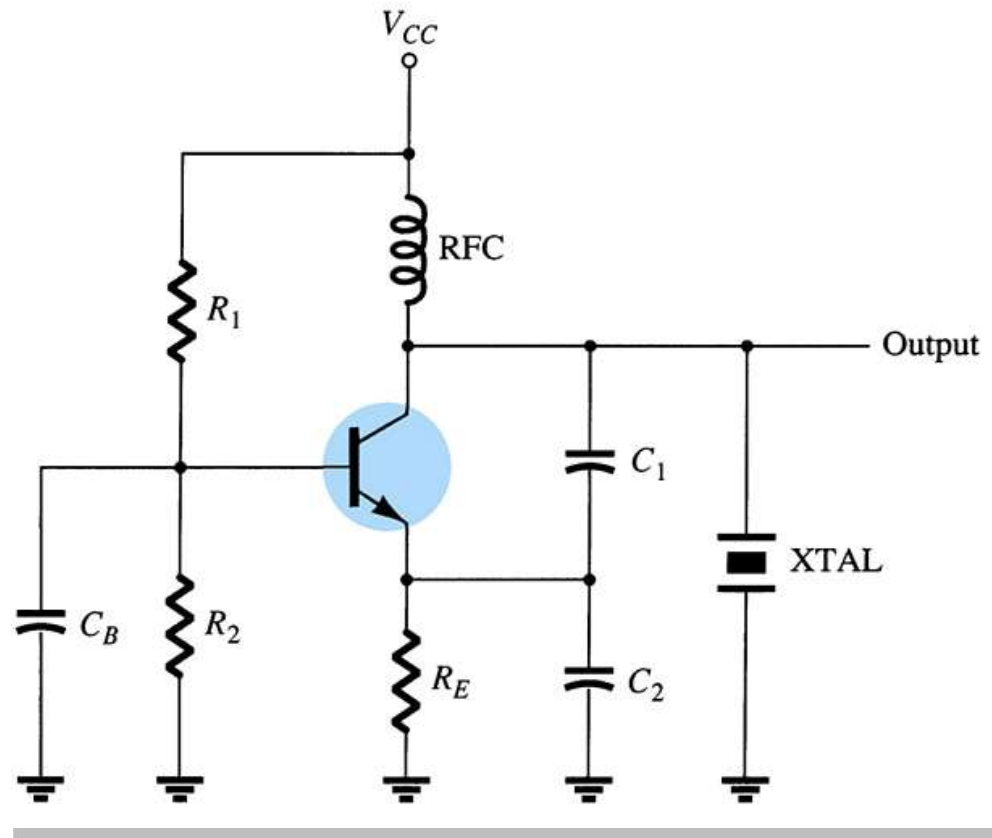
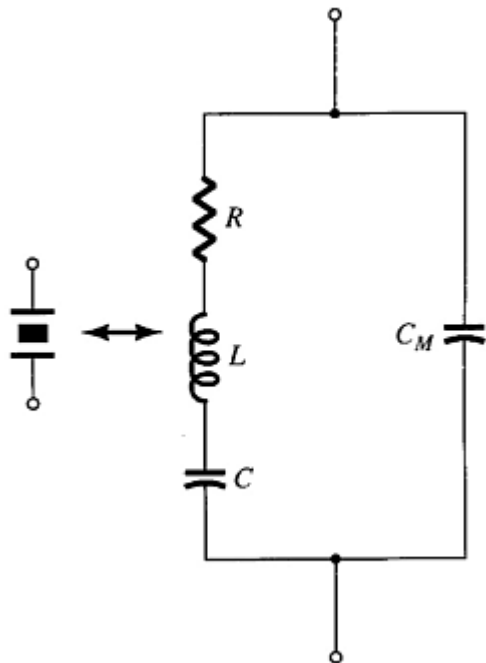
# Series-Resonant Crystal Oscillator

- RLC determine the resonant frequency
- The crystal has a low impedance at the series resonant frequency



# Parallel - Resonant Crystal Oscillator

- RLC and  $C_M$  determine the resonant frequency
- The crystal has a high impedance at parallel resonance



# 3. Relaxation Oscillators

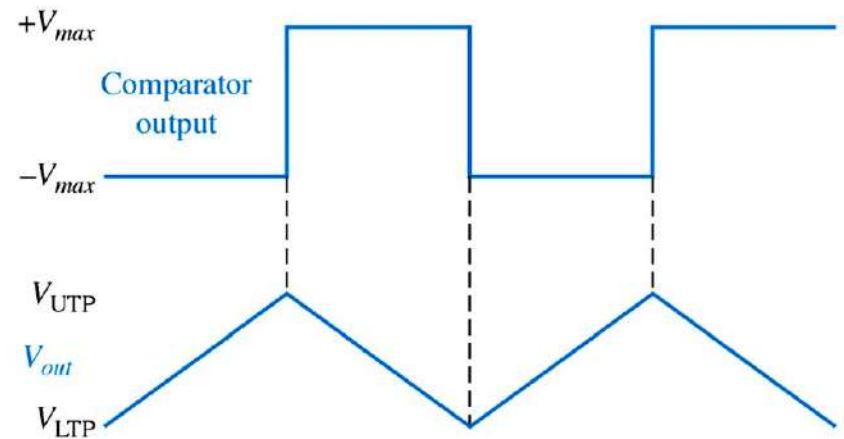
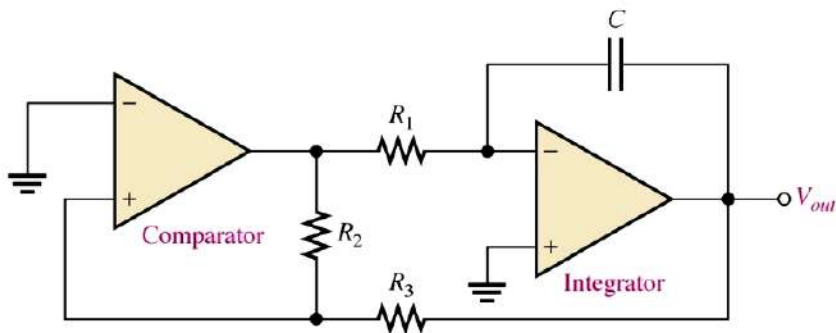
# Relaxation Oscillator

Relaxation oscillators make use of an RC timing and a device that changes states to generate a periodic waveform (non-sinusoidal) such as:

1. Triangular-wave
2. Square-wave
3. Sawtooth

# Triangular-wave Oscillator

Triangular-wave oscillator circuit is a combination of a comparator and integrator circuit.



$$f_r = \frac{1}{4CR_1} \left( \frac{R_2}{R_3} \right)$$

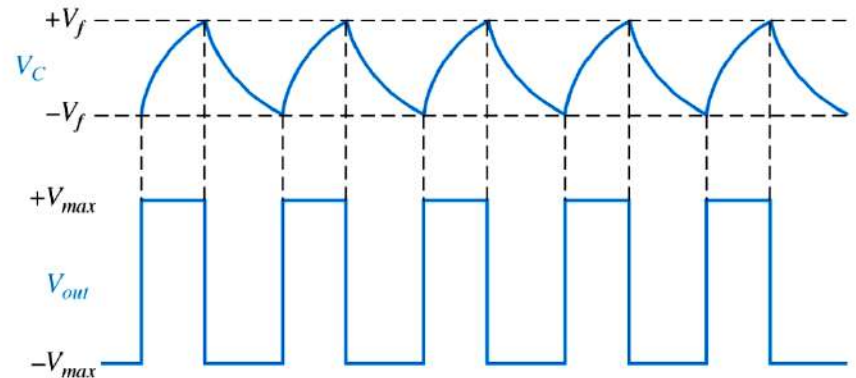
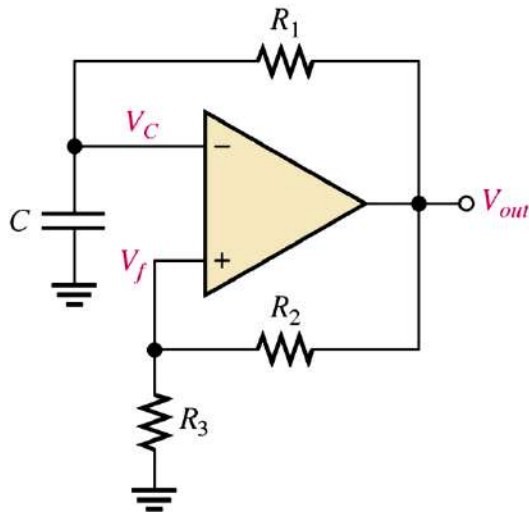
$$V_{UTP} = +V_{\max} \left( \frac{R_3}{R_2} \right)$$

$$V_{LTP} = -V_{\max} \left( \frac{R_3}{R_2} \right)$$



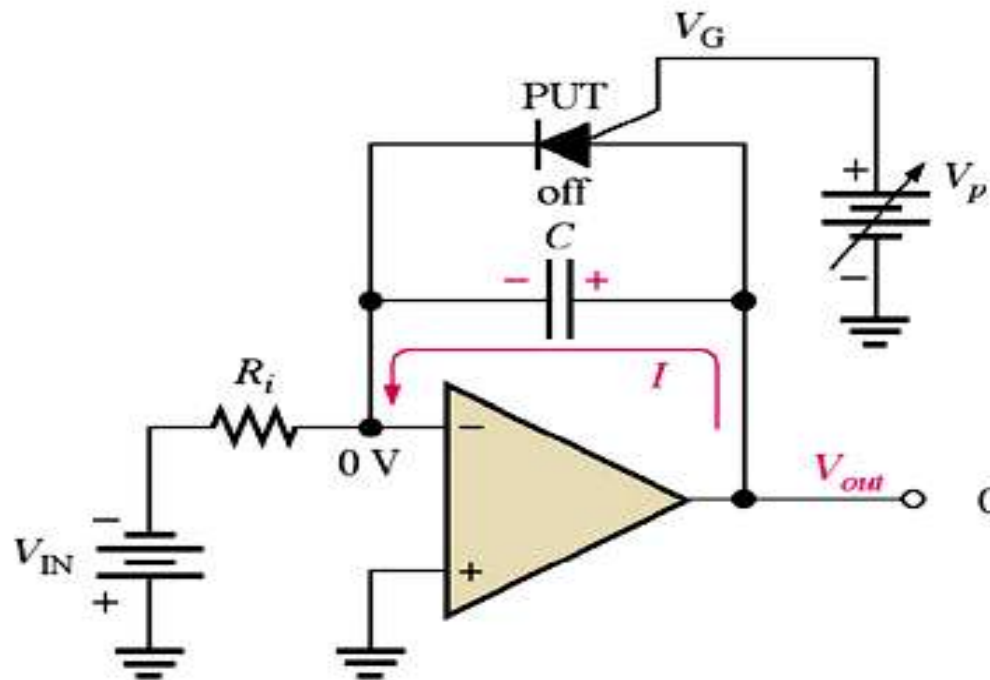
# Square-wave Oscillator

- ❖ A square wave relaxation oscillator is like the Schmitt trigger or Comparator circuit.
- ❖ The charging and discharging of the capacitor cause the op-amp to switch states rapidly and produce a square wave.
- ❖ The RC time constant determines the frequency.



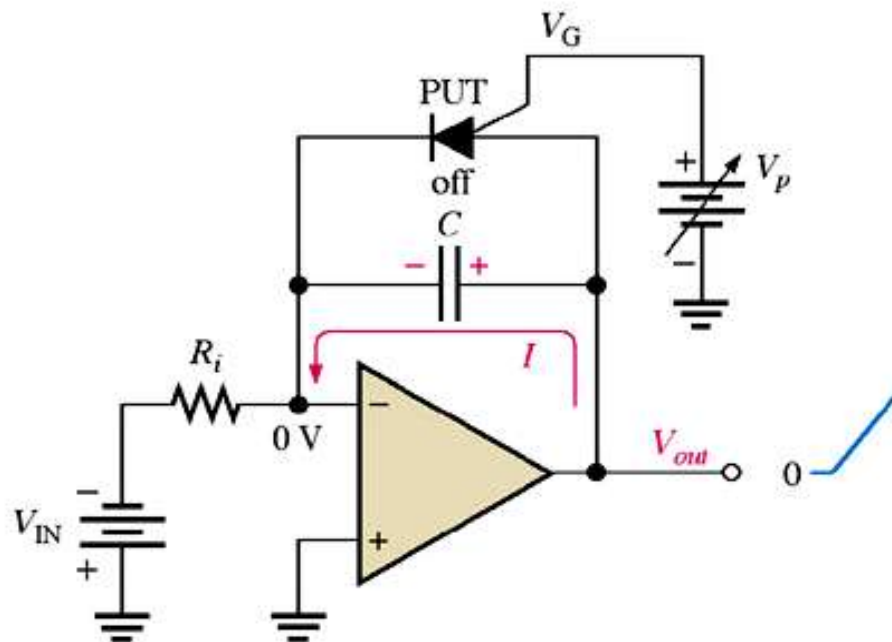
# Sawtooth Voltage-Controlled Oscillator (VCO)

Sawtooth VCO circuit is a combination of a Programmable Unijunction Transistor (PUT) and integrator circuit.



# Sawtooth Voltage-Controlled Oscillator (VCO)

## Operation



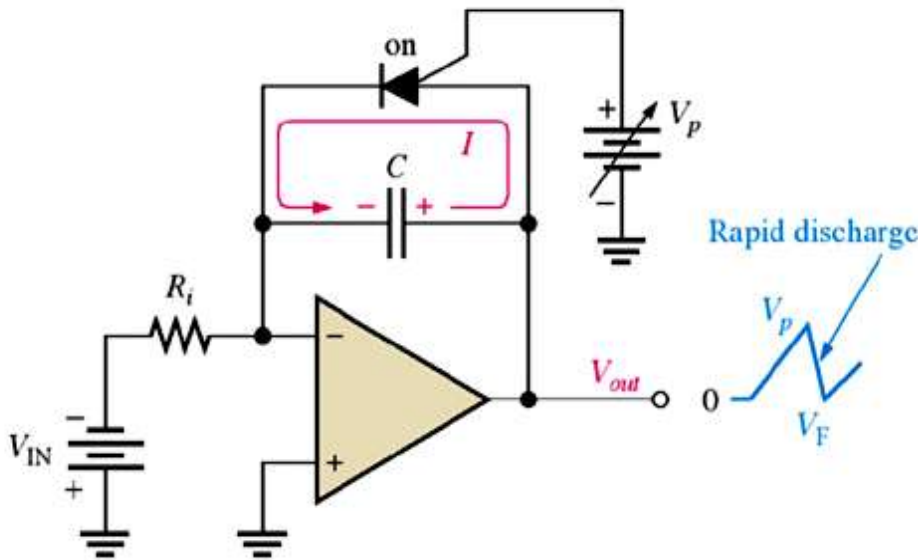
(a) Initially, the capacitor charges, the output ramp begins, and the PUT is off.

Initially, dc input =  $-V_{IN}$

- Volt =  $0V$ ,  $V_{anode} < V_G$
- The circuit is like an integrator.
- Capacitor is charging.
- Output is increasing positive going ramp.

# Sawtooth Voltage-Controlled Oscillator (VCO)

## Operation



(b) The capacitor rapidly discharges when the PUT momentarily turns on.

When  $V_{out} = V_P$

- $V_{anode} > V_G$ , PUT turn 'ON'
- The capacitor rapidly discharges.
- $V_{out}$  drop until  $V_{out} = V_F$ .
- $V_{anode} < V_G$ , PUT turn 'OFF'

$V_P$ -maximum peak value

$V_F$ -minimum peak value

# Sawtooth Voltage-Controlled Oscillator (VCO)

Oscillation frequency is

$$f = \frac{V_{IN}}{R_i C} \left( \frac{1}{V_P - V_F} \right)$$

# Summary

- Sinusoidal oscillators operate with positive feedback.
- Two conditions for oscillation are  $0^\circ$  feedback phase shift and feedback loop gain of 1.
- The initial startup requires the gain to be momentarily greater than 1.
- RC oscillators include the Wien-bridge and phase shift.
- LC oscillators include the Crystal Oscillator.

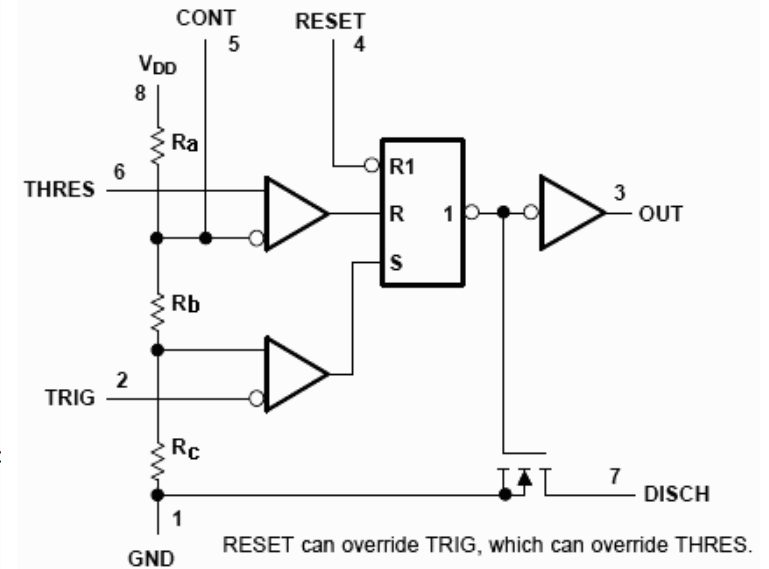
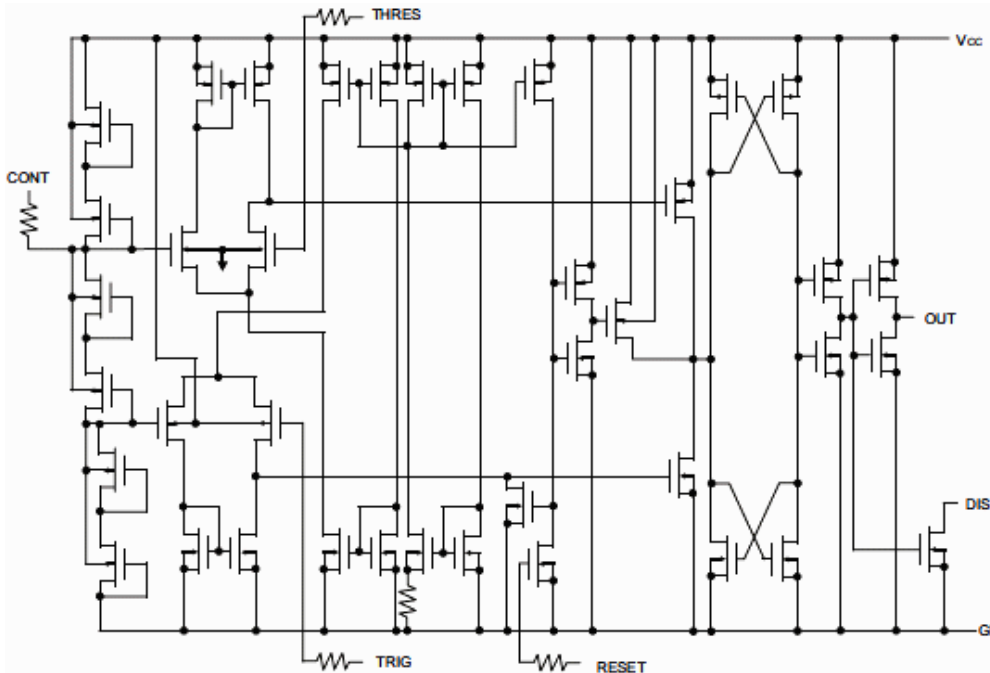
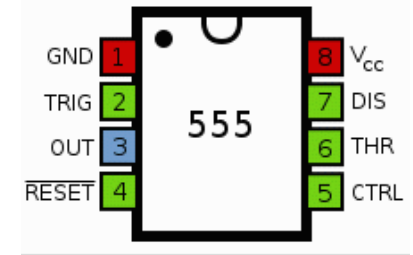
# Summary

- The crystal actually uses a crystal as the LC tank circuit and is very stable and accurate.
- A voltage controlled oscillator's (VCO) frequency is controlled by a dc control voltage.

# LM/TLC 555 Timer



# The TLC555C Chip (in your kit)



# LM555 Timer Chip (TTL)

## TLC555C Timer Chip (CMOS)

- An integrated chip that is used in a wide variety of circuits to generate square wave and triangular shaped single and periodic pulses.
  - Examples in your home are
    - high efficiency LED and fluorescence light dimmers and
    - temperature control systems for electric stoves
    - tone generators for appliance “beeps”
  - The Application Notes section of the datasheets for the TLC555 and LM555 timers have a number of other circuits that are in use today in various communications and control circuits.

## Terms you may see in 555 circuits:

- **Astable** – a circuit that can not remain in one state.
- **Monostable** – a circuit that has one stable state. When perturbed, the circuit will return to the stable state.
- **One Shot** – Monostable circuit that produces one pulse when triggered.
- **Flip Flop** – a digital circuit that flips or toggles between two stable states (bistable). The Flip Flop inputs decide which of the two states its output will be.
- **Multivibrator** – a circuit used to implement a simple two-state system, which may be astable, monostable, or bistable.
- **CMOS** – complimentary Mosfet logic. CMOS logic dominates the digital industry because the power requirements and component density are significantly better than other technologies.

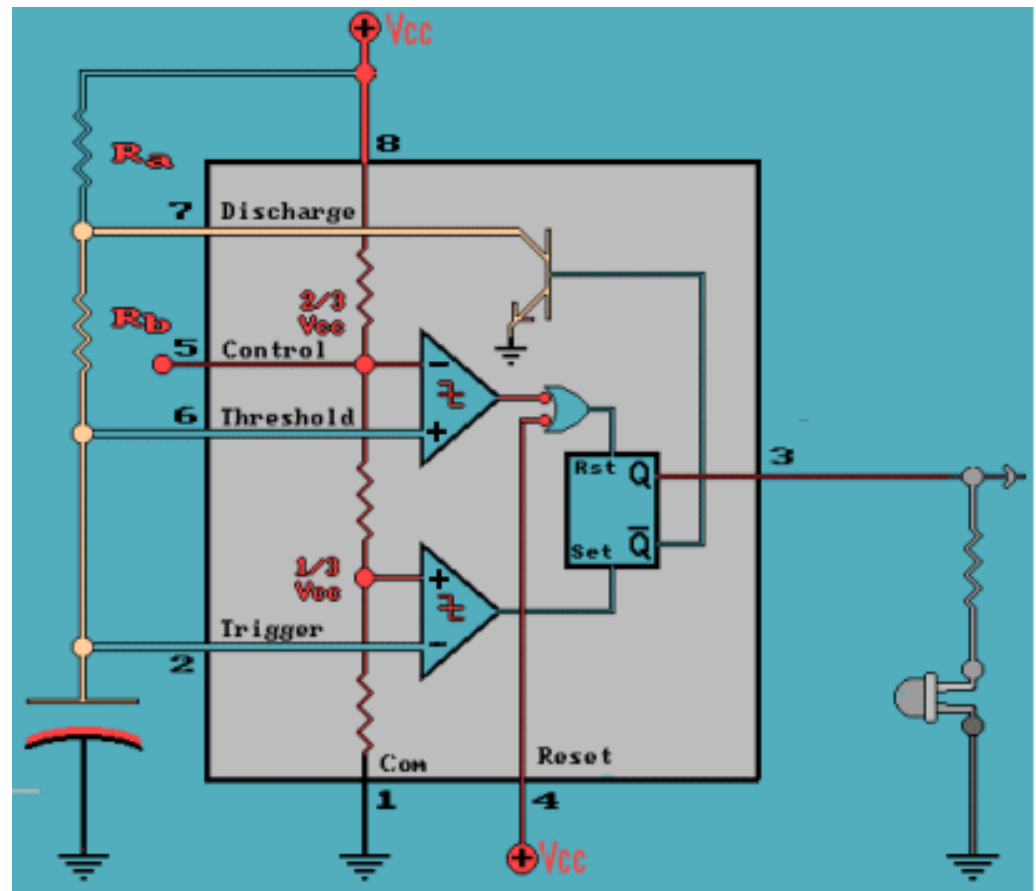
# Two Types of 555 Multivibrators

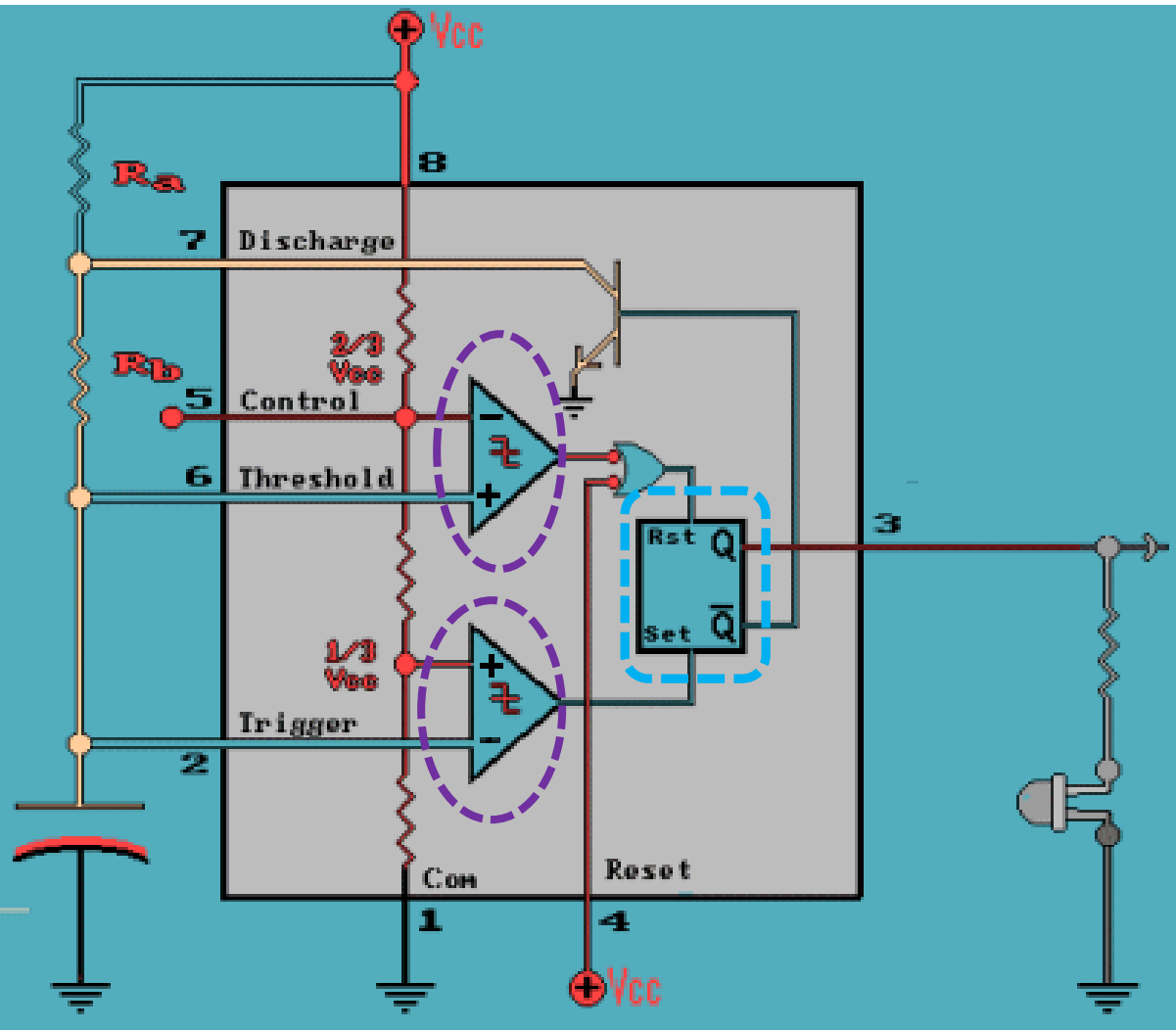
- Monostable
  - A single pulse is outputted when an input voltage attached to the trigger pin of the 555 timer equals the voltage on the threshold pin.
- Astable
  - A periodic square wave is generated by the 555 timer.
    - The voltage for the trigger and threshold pins is the voltage across a capacitor that is charged and discharged through two different RC networks.

I know – who comes up with these names?

# How a 555 Timer Works

- We will operate the 555 Timer as an Astable Multivibrator in the circuit for the metronome.





The components that make up a 555 timer are shown within the gray box.

Internal resistors form a voltage divider that provides  $\frac{1}{3}V_{CC}$  and  $\frac{2}{3}V_{CC}$  reference voltages.

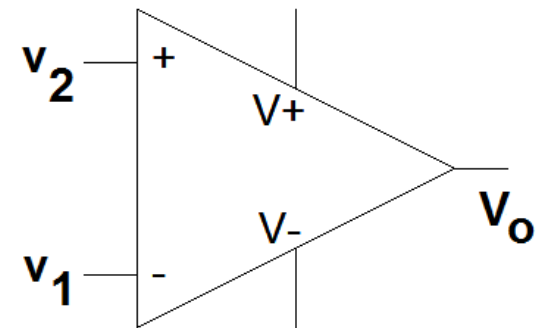
Two internal **voltage comparators** determine the state of a **D flip-flop**.

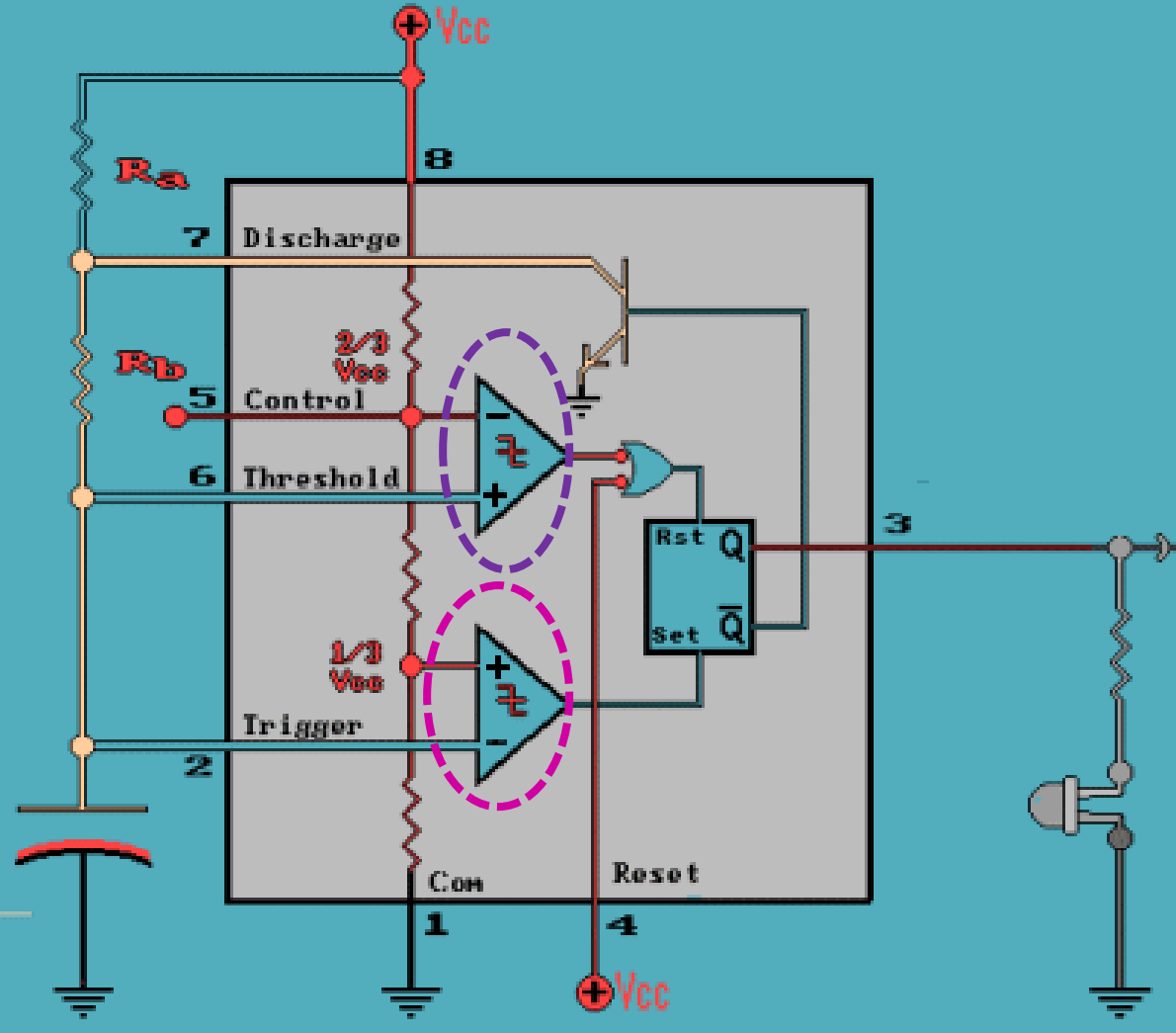
The flip-flop output controls a transistor switch.

[http://www.williamson-labs.com/480\\_555.htm](http://www.williamson-labs.com/480_555.htm)

# Voltage Comparator

- As a reminder, an Op Amp without a feedback component is a voltage comparator.
  - Output voltage changes to force the negative input voltage to equal the positive input voltage.
    - A maximum output voltage ( $V_o$ ) is against the positive supply rail ( $V+$ ) if the positive input voltage ( $v_2$ ) is greater than negative input voltage ( $v_1$ ).
    - A minimum output voltage ( $V_o$ ) is against the negative supply rail ( $V-$ ) if the negative input voltage ( $v_1$ ) is greater than the positive input voltage ( $v_2$ ).





The voltage comparators use the internal voltage divider to keep the capacitor voltage ( $V_C$ ) between  $\frac{1}{3}V_{CC}$  and  $\frac{2}{3}V_{CC}$ .

The output of the **lower voltage comparator** will be high ( $V_{CC}$ ) when  $V_C < \frac{1}{3}V_{CC}$ , and low (0 V) when  $V_C > \frac{1}{3}V_{CC}$

( $\frac{1}{3}V_{CC}$  = the voltage across the lower resistor in the internal voltage divider).

The output of the **upper voltage comparator** will be low (0 V) when  $V_C < \frac{2}{3}V_{CC}$ , and high ( $V_{CC}$ ) when  $V_C > \frac{2}{3}V_{CC}$

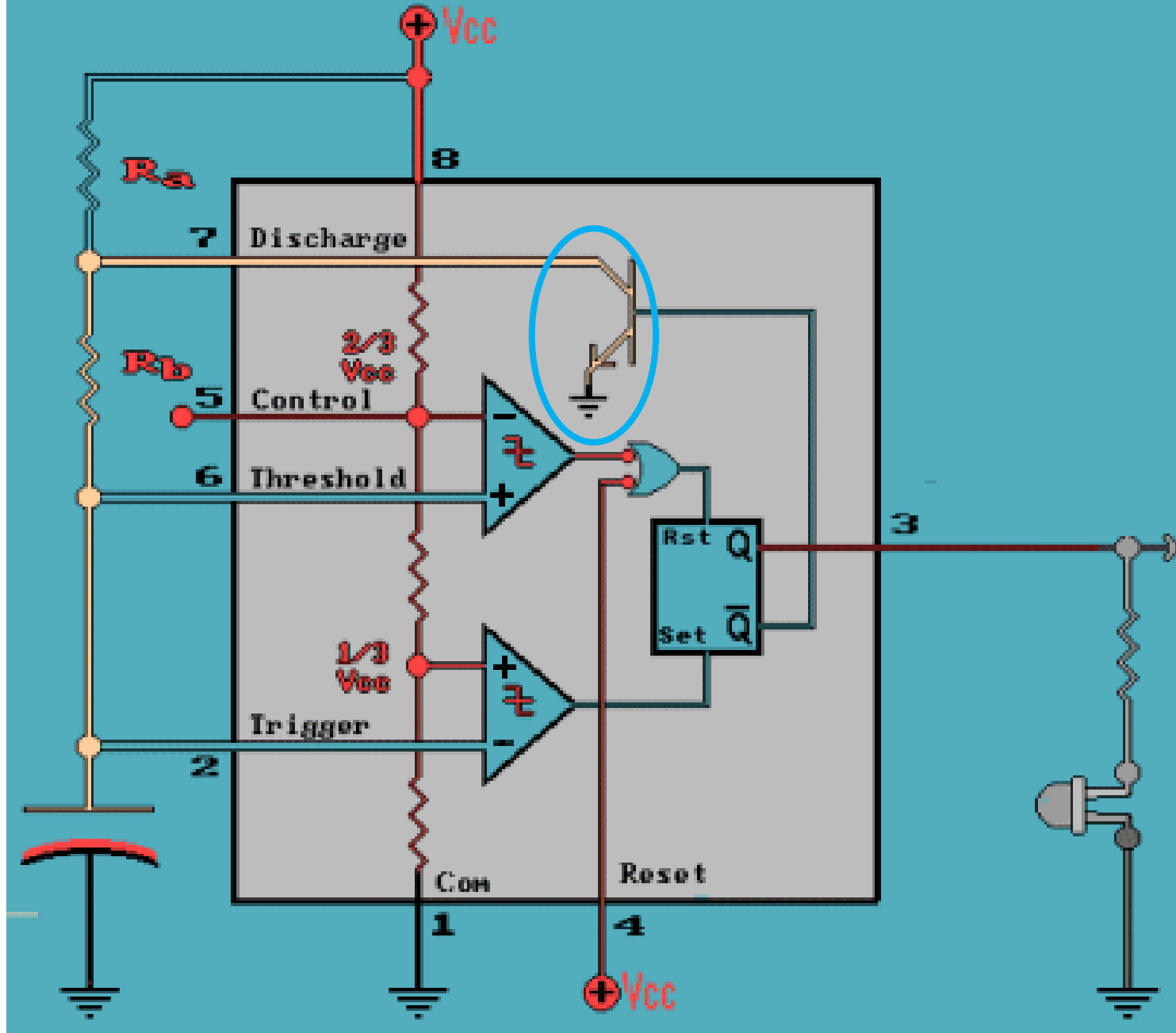
( $\frac{2}{3}V_{CC}$  = the voltage across the two lower resistors in the internal voltage divider).

[http://www.williamson-labs.com/480\\_555.htm](http://www.williamson-labs.com/480_555.htm)



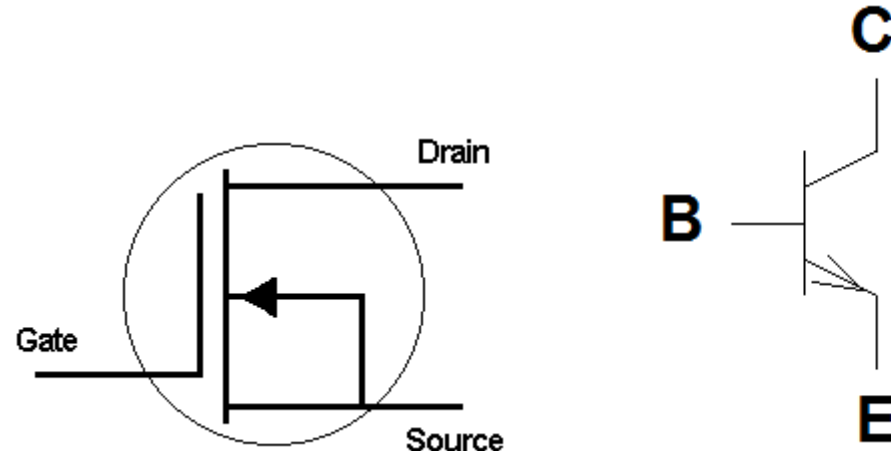
The bipolar transistor (BJT) acts as a switch.

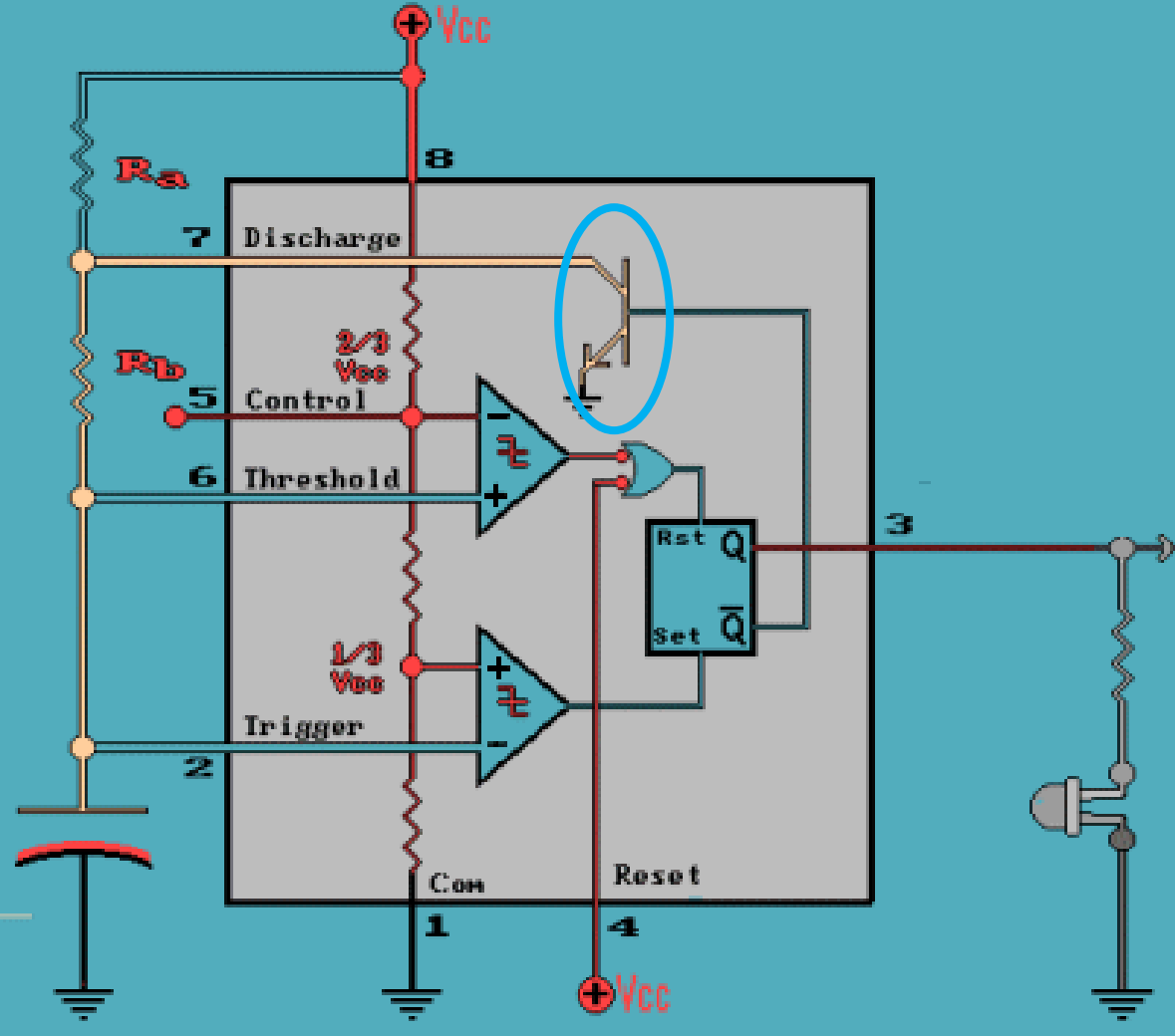
NOTE: Your kit TLC555 uses a MOSFET instead of a BJT.



# Transistor

- As you will learn in ECE 2204, a BJT or MOSFET transistor can be connected to act like a switch.
  - When a positive voltage is applied to the base or gate, the transistor acts like there is a very small resistor is between the collector and the emitter, or the drain and the source.
  - When ground is applied to the base or gate, the transistor acts like there is a an open circuit between the collector and the emitter, or the drain and the source.





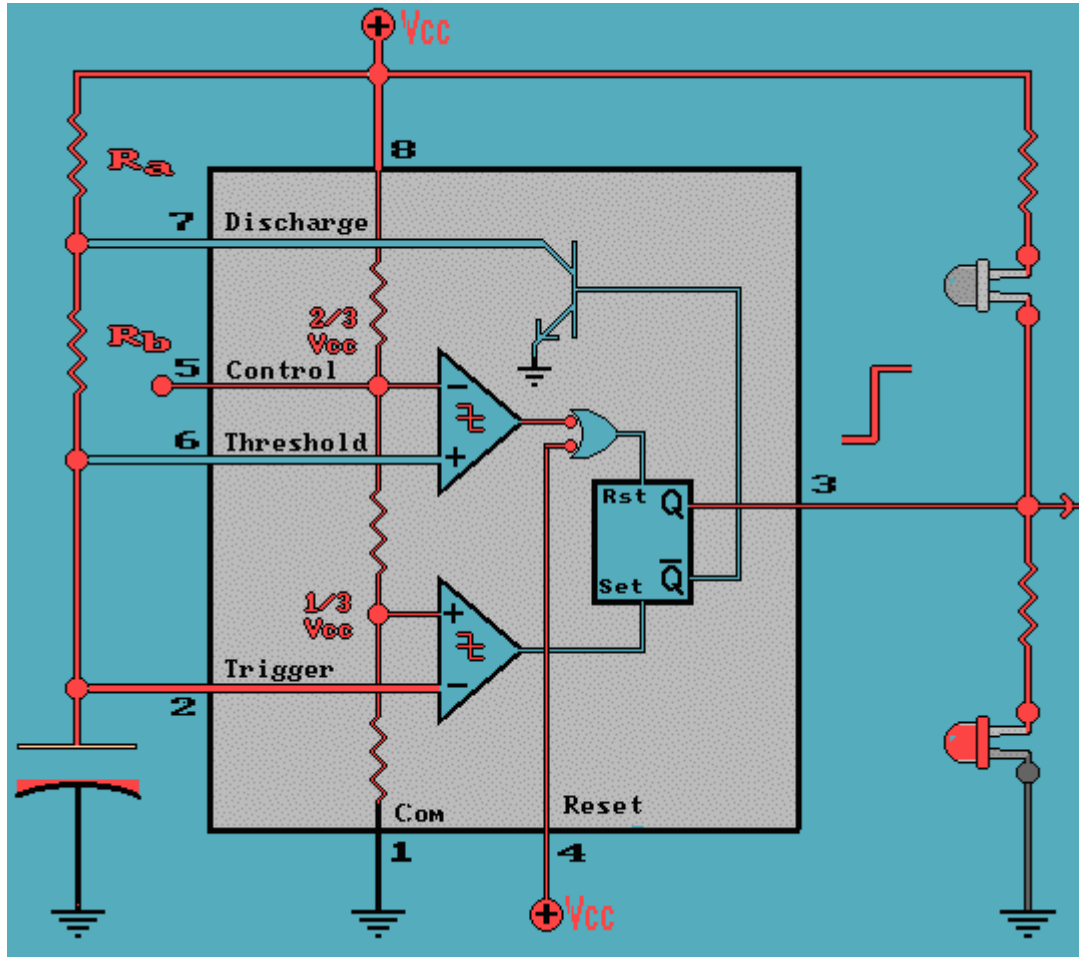
The **transistor** inside the 555 switches the discharge pin (7) to ground (or very close to 0 V), when  $Q_{\text{bar}}$  (the Q with a line over it) of the D flip-flop is high ( $V_{Q_{\text{bar}}} \approx V_{CC}$ ).

The transistor grounds the node between external timing resistors  $R_a$  and  $R_b$ . The capacitor discharges through  $R_b$  to ground through the transistor. *Current through  $R_a$  also goes to ground through the transistor.*

When the transistor is switched off, it acts like an open circuit.  $V_{CC}$  now charges the capacitor through  $R_a$  and  $R_b$ .

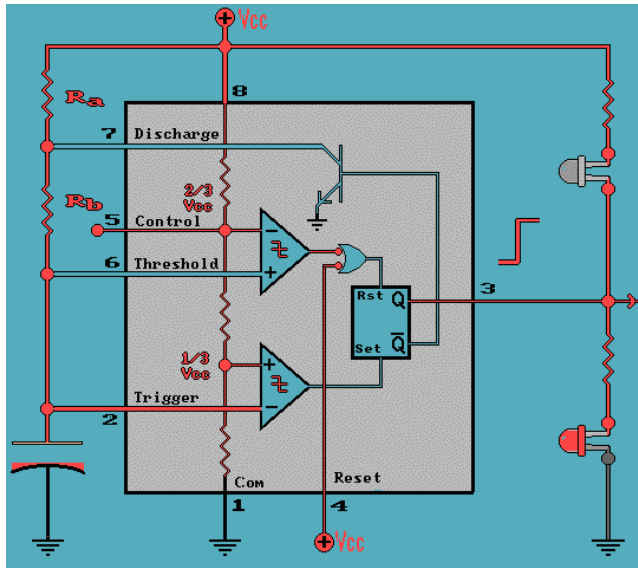
[http://www.williamson-labs.com/480\\_555.htm](http://www.williamson-labs.com/480_555.htm)

# When you first apply power to the 555



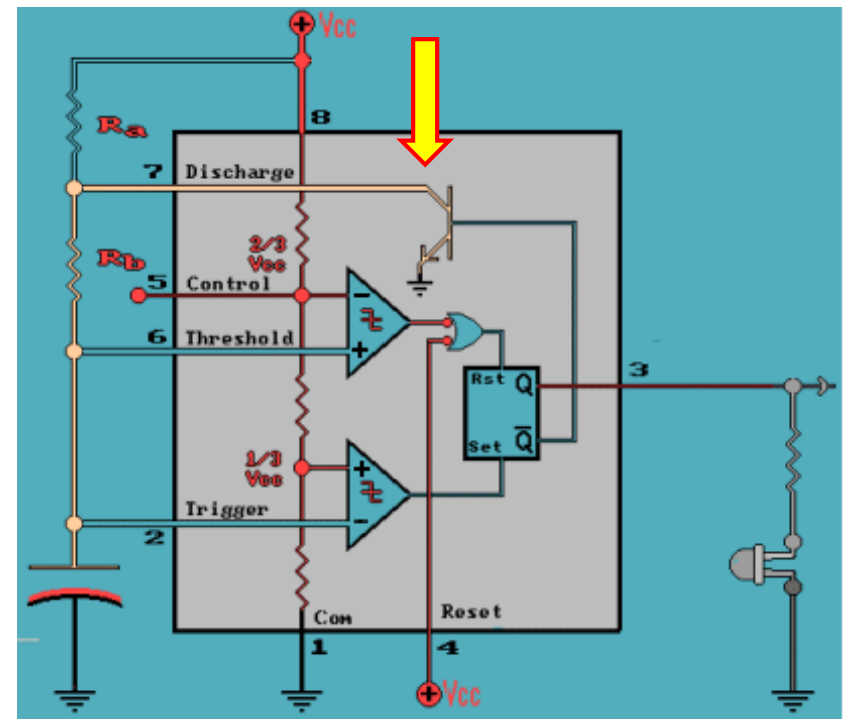
- The capacitor charges through  $R_A$  and  $R_B$ .
- Because  $V_C$  started 0 V, the first timing period will be longer than the periods that follow.

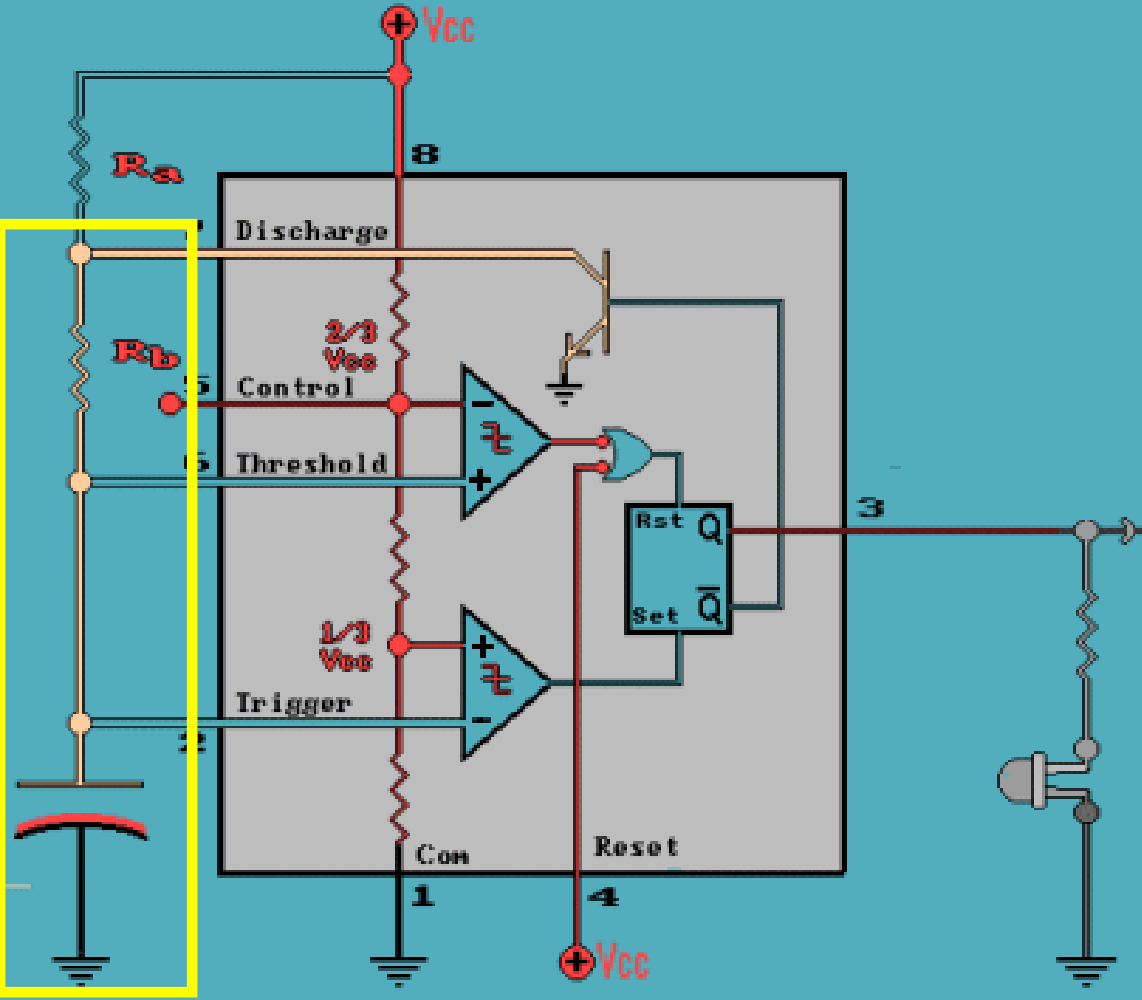
# Charging



- The capacitor charges through  $R_a$  and  $R_b$  until  $V_C = \frac{2}{3}V_{CC}$ .

- ▶ When  $V_C$  reaches  $\frac{2}{3}V_{CC}$ , the output of the upper voltage comparator changes and resets the D flip-flop,  $Q$  switches to high ( $\approx V_{CC}$ ), and the transistor switches on.
- ▶ The capacitor then begins discharging through  $R_b$  & the transistor to ground.





## Discharging:

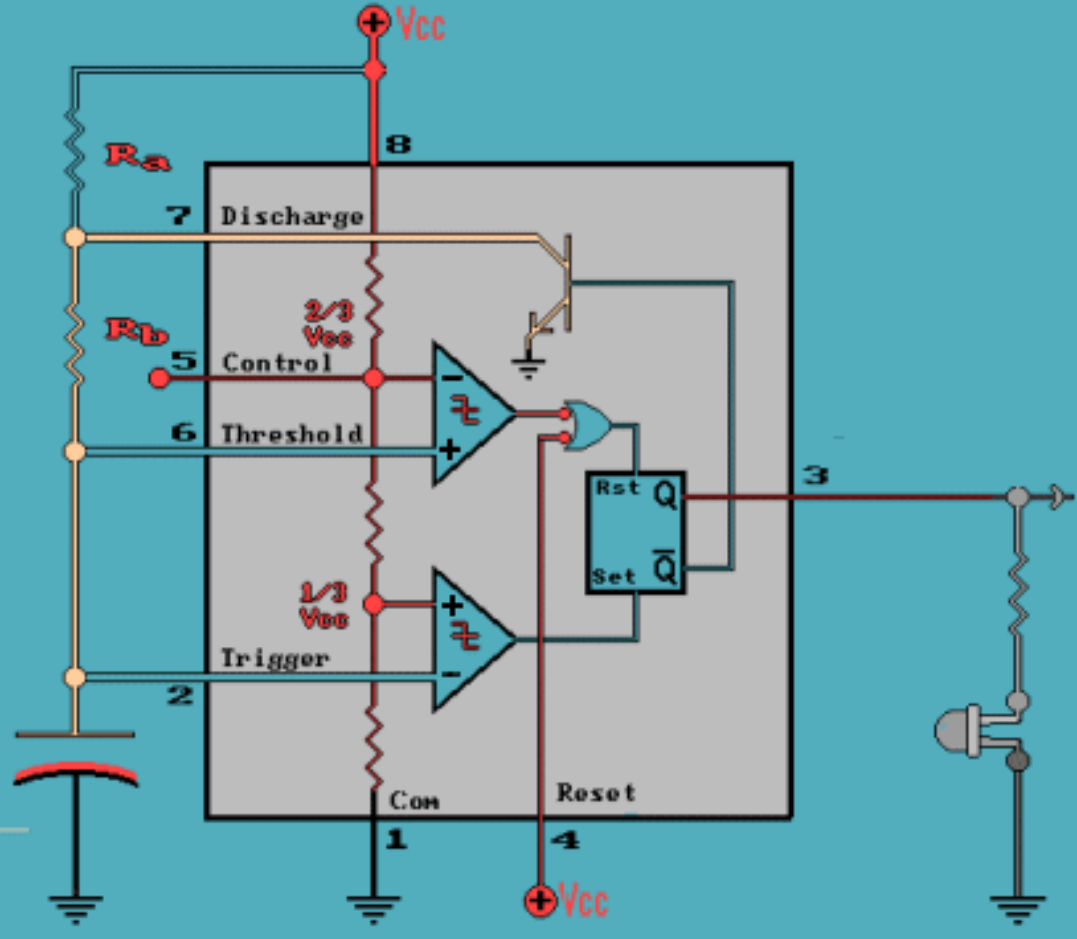
The capacitor discharges through  $R_b$  and the transistor to ground.

Current through  $R_a$  is also grounded by the transistor.

- ▶ When  $V_C$  reaches  $\frac{1}{3}V_{CC}$ , the output of the lower voltage comparator changes and sets the D flip-flop,  $Q_{bar}$  switches to low ( $\approx 0$  V), and the transistor switches off.
- ▶ The capacitor then begins charging through  $R_a$  and  $R_b$ .

[http://www.williamson-labs.com/480\\_555.htm](http://www.williamson-labs.com/480_555.htm)

Thus, the voltage of the capacitor can be no more than  $\frac{2}{3}V_{CC}$  and no less than  $\frac{1}{3}V_{CC}$  if all of the components internal and external to the 555 are ideal.



The output of the 555 timer, pin 3, is Q on the D flip-flop.

- When Qbar is 5 V and the capacitor is charging, Q is 0 V.
- When Qbar is 0 V and the capacitor is discharging, Q is 5 V.

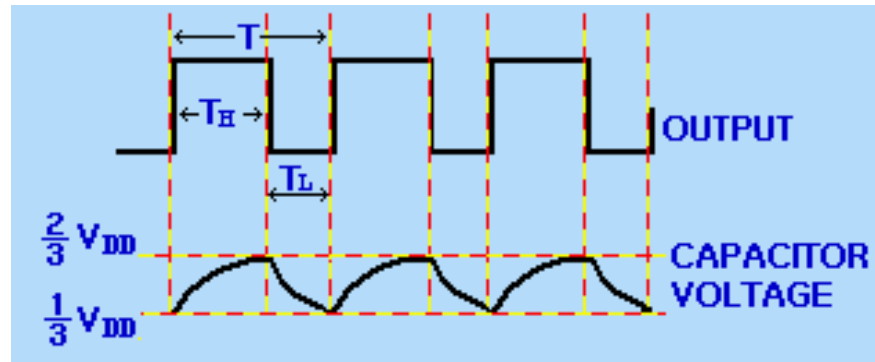
Thus, the output of a 555 timer is a continuous square wave function (0 V to 5 V) where:

- the period is dependent the sum of the time it takes to charge the capacitor to  $\frac{2}{3}V_{CC}$  and the time that it takes to discharge the capacitor to  $\frac{1}{3}V_{CC}$ .
- In this circuit, the only time that the duty cycle (the time that the output is at 0 V divided by the period) will be 0.5 (or 50%) is when  $R_a = 0 \Omega$ , which should not be allowed to occur as that would connect  $V_{cc}$  directly to ground when the transistor switches on.

[http://www.williamson-labs.com/480\\_555.htm](http://www.williamson-labs.com/480_555.htm)

# Astable Multivibrator - Waveforms

- $T_H$  is the time it takes C to charge from  $\frac{1}{3}V_{CC}$  to  $\frac{2}{3}V_{CC}$ 
  - $T_H = (R_a + R_b) * C * [-\ln(\frac{1}{2})]$  (from solving for the charge time between voltages)
- $T_L$  is the time it takes C to discharge from  $\frac{2}{3}V_{CC}$  to  $\frac{1}{3}V_{CC}$ 
  - $T_{Low} = R_b * C * [-\ln(\frac{1}{2})]$  (from solving for the charge time between voltages)
- The duty cycle (% of the time the output is high) depends on the resistor values.



- Williamson Labs [555 astable circuit waveform animation](#)

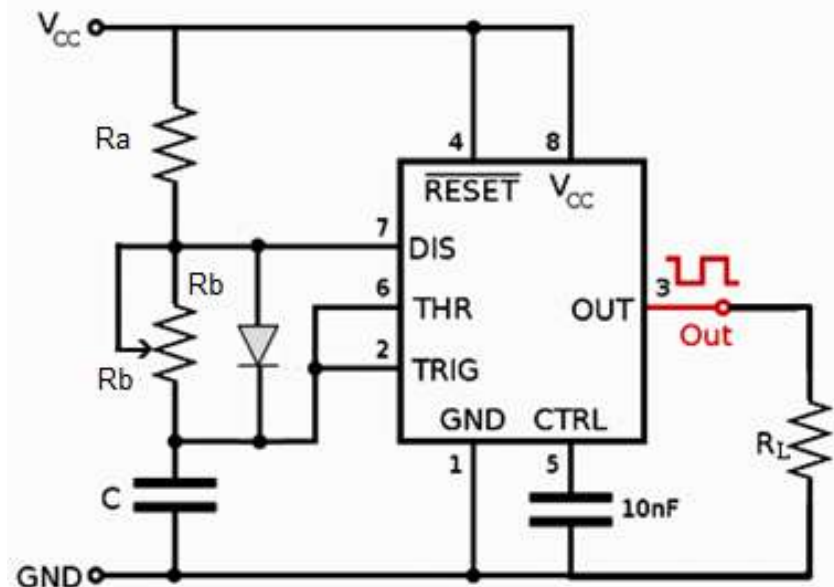


# Shortening the Astable Duty Cycle

- The duty cycle of the standard 555 timer circuit in Astable mode must be greater than 50%.
  - $T_{\text{high}} = 0.693(R_a + R_b)C$  [C charges through  $R_a$  and  $R_a$  from  $V_{CC}$ ]
  - $T_{\text{low}} = 0.693R_b C$  [C discharges through  $R_b$  into pin 7]
  - $R_1$  must have a resistance value greater than zero to prevent the discharge pin from directly shorting  $V_{DD}$  to ground.
  - Duty cycle =  $T_{\text{high}} / (T_{\text{high}} + T_{\text{low}}) = (R_a + R_b) / (R_a + 2R_b) > 50\%$  if  $R_a \neq 0$

- **Adding a diode across  $R_b$**  allows the capacitor to charge directly through  $R_a$ .

This sets  $T_{\text{high}} \approx 0.693R_a C$   
 $T_{\text{low}} = 0.693R_b C$  (unchanged)



# Useful 555 Timer Chip Resources

- [TI Data Sheets and design info](#)
  - [Data Sheet](#) (pdf)
  - [Design Calculator](#) (zip)
- Williamson Labs [http://www.williamson-labs.com/480\\_555.htm](http://www.williamson-labs.com/480_555.htm)
  - Timer tutorials with a 555 astable circuit waveform animation.
  - Philips App Note [AN170](#) (pdf)
- [Wikipedia - 555 timer IC](#)
- NE555 Tutorials <http://www.unitechelectronics.com/NE-555.htm>
- Doctronics 555 timer tips <http://www.doctronics.co.uk/555.htm>
- The Electronics Club <http://www.kpsec.freeuk.com/555timer.htm>
- 555 Timer Circuits <http://www.555-timer-circuits.com>
- 555 Timer Tutorial <http://www.sentex.net/~mec1995/gadgets/555/555.html>
- Philips App Note AN170 [http://www.doctronics.co.uk/pdf\\_files/555an.pdf](http://www.doctronics.co.uk/pdf_files/555an.pdf)

# Equations

- Time constants of two different resistor-capacitor networks determine the length of time the timer output,  $t_1$  and  $t_2$ , is at 5V and 0V, respectively.

$$t_1 = 0.693(R_a + R_b)C$$

$$t_2 = 0.693(R_b)C$$

# Types of Capacitors

- Fixed Capacitors

- Nonpolarized

- May be connected into circuit with either terminal of capacitor connected to the high voltage side of the circuit.

- Insulator: Paper, Mica, Ceramic, Polymer

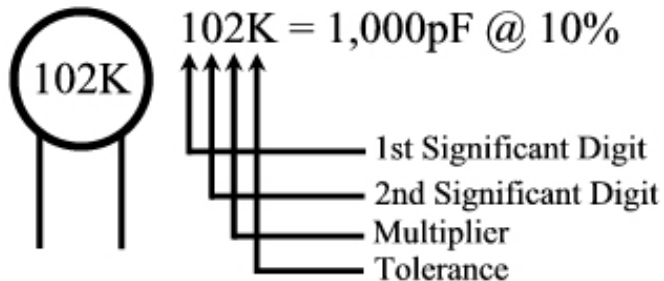
- Electrolytic

- The negative terminal must always be at a lower voltage than the positive terminal

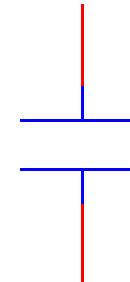
- Plates or Electrodes: Aluminum, Tantalum

# Nonpolarized

- It's difficult to make nonpolarized capacitors that store a large amount of charge or operate at high voltages.
  - Tolerance on capacitance values is very large
    - +50%/-25% is not unusual



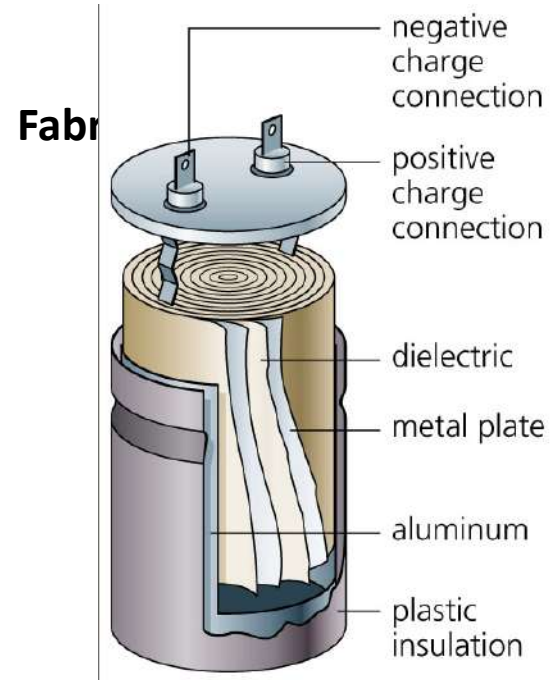
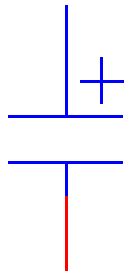
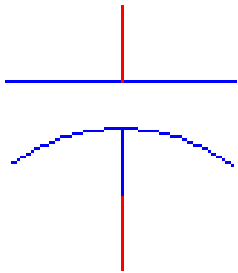
PSpice Symbol



[http://www.marvac.com/fun/ceramic\\_capacitor\\_codes.aspx](http://www.marvac.com/fun/ceramic_capacitor_codes.aspx)

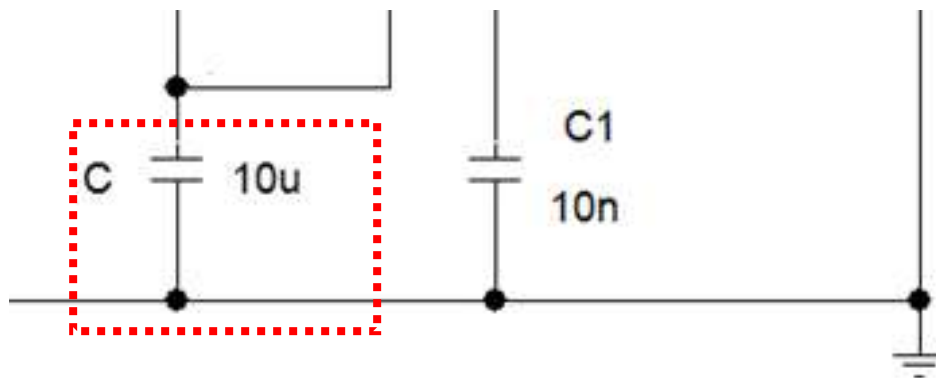
# Electrolytic

## Pspice Symbols



# Electrolytic Capacitors

- The negative electrode must always be at a lower voltage than the positive electrode.
  - So in your circuit, the negative electrode must be grounded.



# Frequency and Duty Cycle

$$f = \frac{1}{t_1 + t_2} = \frac{1.44}{(R_a + 2R_b)C}$$

$$D = \frac{t_2}{t_1 + t_2} = \frac{R_b}{R_a + 2R_b}$$

When the output of the 555 timer changes from 5V to 0V, a pulse current will flow through the speaker, causing the speaker to create a click sound. You will change the frequency of the pulses to the speaker by changing the value of  $R_a$ . Since  $R_a$  is usually much larger than  $R_b$ , the frequency of the pulses are linearly proportional to the value of  $R_a$  and the duty cycle of the pulse waveform will be very short.



# Active Filters

# Introduction

- Filters are circuits that are capable of *passing signals within a band* of frequencies while *rejecting or blocking* signals of frequencies *outside this band*. This property of filters is also called “frequency selectivity”.
- Filter can be passive or active filter.

**Passive filters:** The circuits built using RC, RL, or RLC circuits.

**Active filters** : The circuits that employ one or more op-amps in the design an addition to resistors and capacitors

# Advantages of Active Filters over Passive Filters

- Active filters can be designed to provide required gain, and hence no attenuation as in the case of passive filters
- No loading problem, because of high input resistance and low output resistance of op-amp.
- Active Filters are cost effective as a wide variety of economical op-amps are available.

# Applications

- Active filters are mainly used in communication and signal processing circuits.
- They are also employed in a wide range of applications such as entertainment, medical electronics, etc.

# Active Filters

➤ There are 4 basic categories of active filters:

**1. Low-pass filters**

**2. High-pass filters**

**3. Band-pass filters**

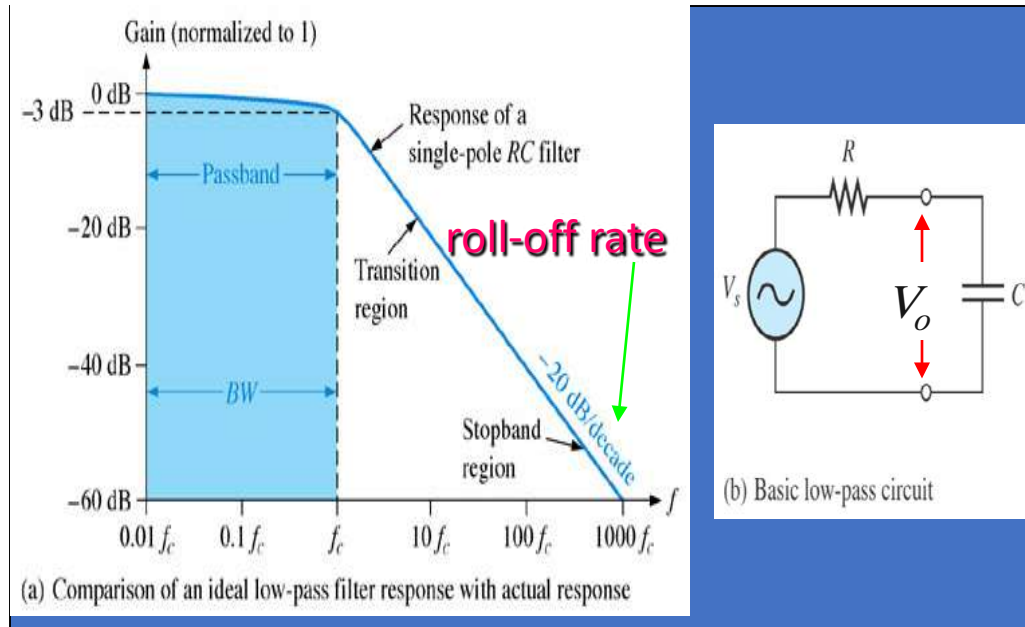
**4. Band-reject filters**

➤ Each of these filters can be built by using op-amp as the active element combined with RC, RL or RLC circuit as the passive elements.

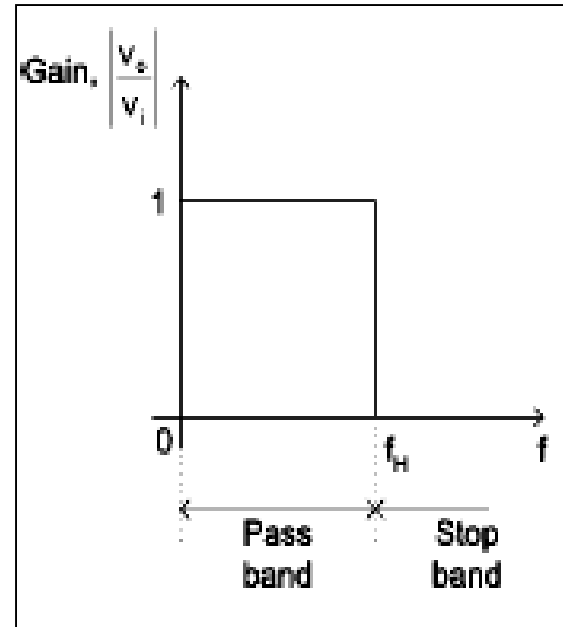
# BASIC FILTER RESPONSES

## Low-Pass Filter Response

- A **low-pass filter** is a filter that passes frequencies from 0Hz to critical frequency,  $f_c$  and significantly attenuates all other frequencies.



Actual response



Ideal response

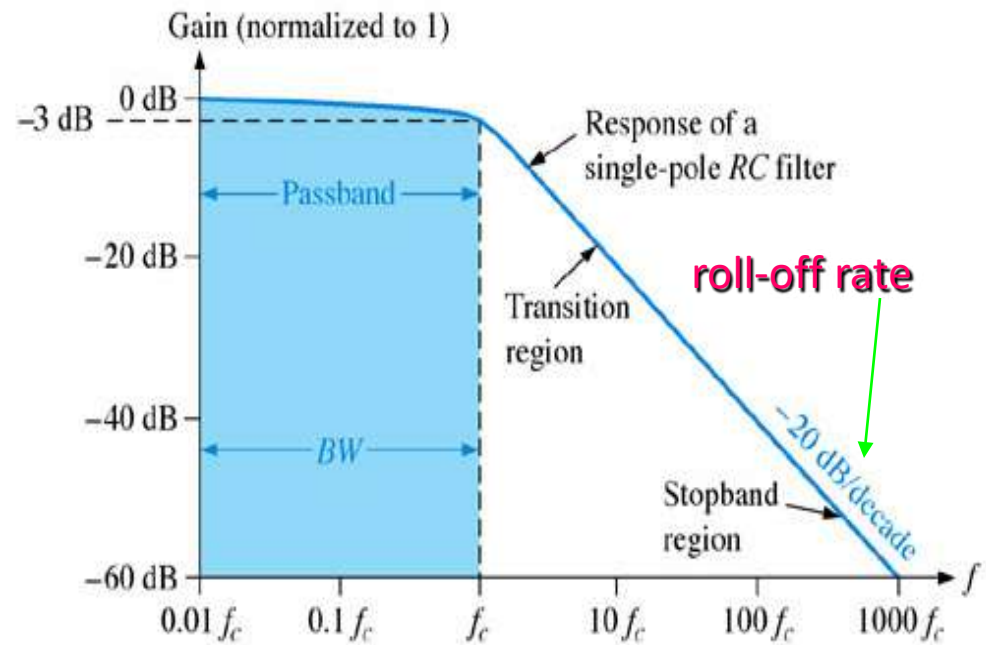
- Ideally, the response drops abruptly at the critical frequency,  $f_H$

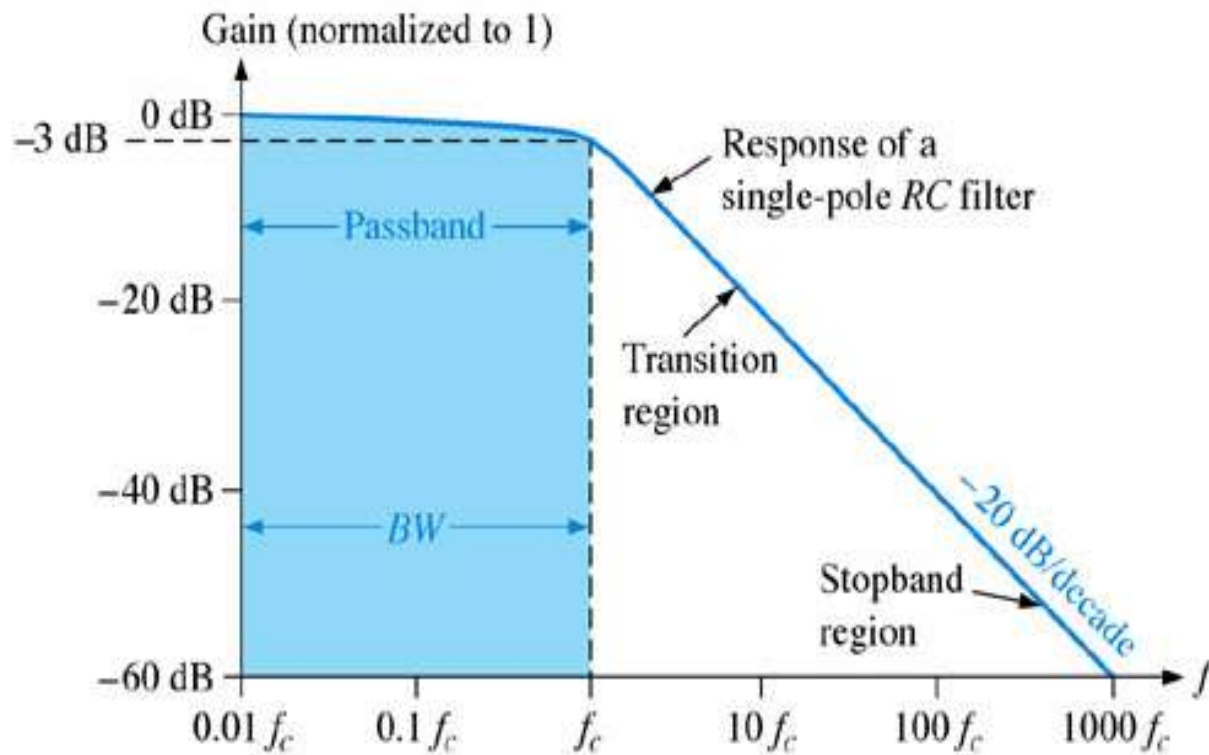
**Passband** of a filter is the range of frequencies that are allowed to pass through the filter with minimum attenuation (usually defined as less than -3 dB of attenuation).

**Transition region** shows the area where the fall-off occurs.

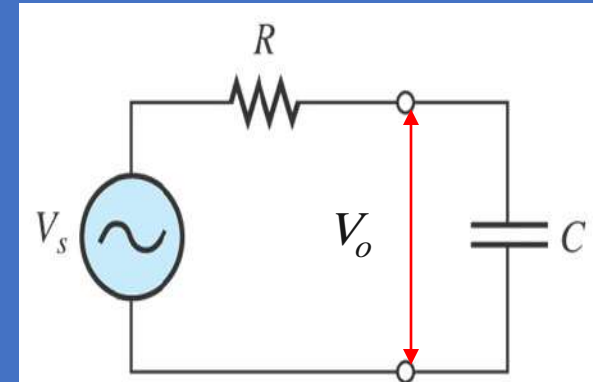
**Stopband** is the range of frequencies that have the most attenuation.

**Critical frequency,  $f_c$** , (also called the cutoff frequency) defines the end of the passband and normally specified at the point where the response drops - 3 dB (70.7%) from the passband response.





(a) Comparison of an ideal low-pass filter response with actual response



(b) Basic low-pass circuit

- At low frequencies,  $X_C$  is very high and the capacitor circuit can be considered as open circuit. Under this condition,  $V_o = V_{in}$  or  $A_V = 1$  (unity).
- At very high frequencies,  $X_C$  is very low and the  $V_o$  is small as compared with  $V_{in}$ . Hence the gain falls and drops off gradually as the frequency is increased.



- The **bandwidth** of an **ideal** low-pass filter is equal to  $f_c$ :

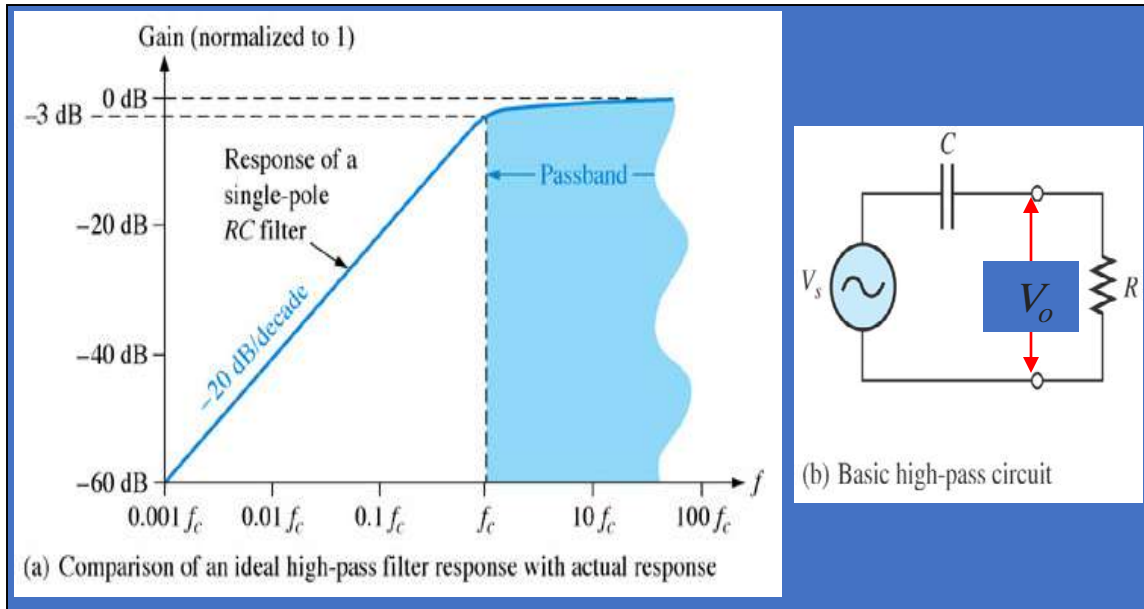
$$BW = f_c$$

- The critical frequency of a low-pass RC filter occurs when  $X_c = R$  and can be calculated using the formula below:

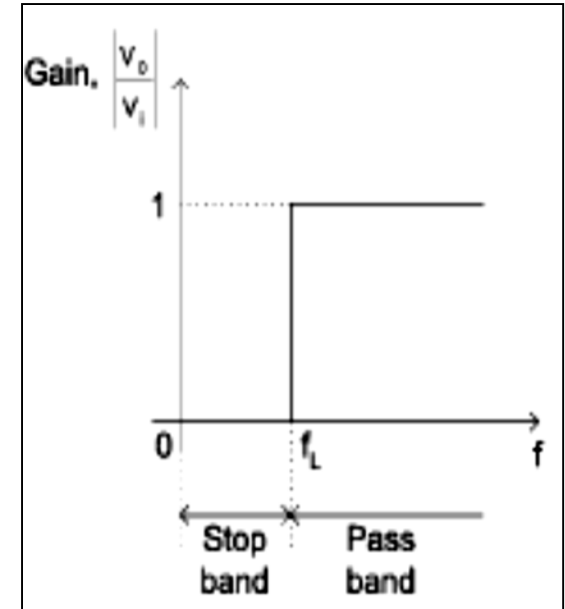
$$f_c = \frac{1}{2\pi RC}$$

# High-Pass Filter Response

- A **high-pass filter** is a filter that significantly attenuates or rejects all frequencies **below**  $f_c$  and passes all frequencies **above**  $f_c$ .
- The passband of a high-pass filter is all frequencies above the critical frequency.



Actual response



Ideal response

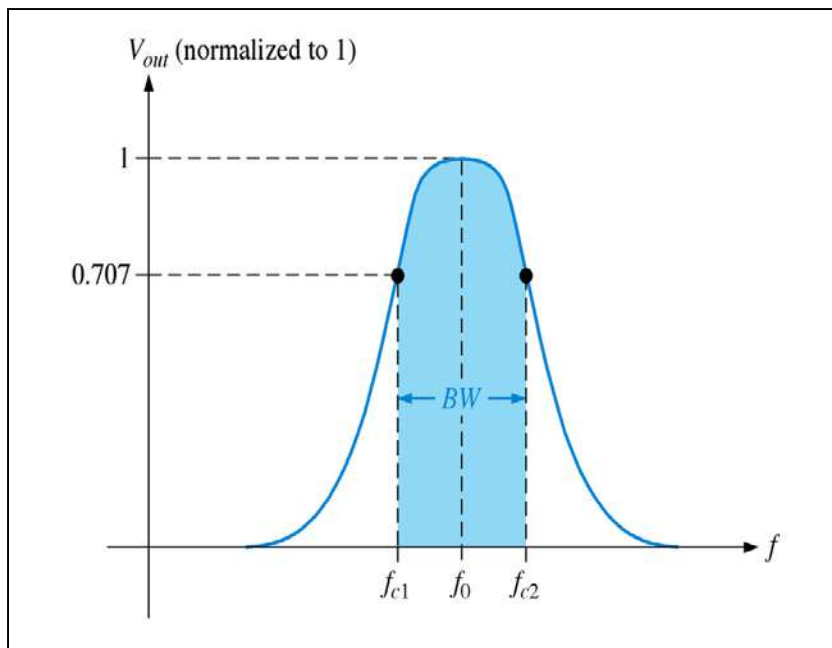
- Ideally, the response rises abruptly at the critical frequency,  $f_L$

- The critical frequency of a high-pass RC filter occurs when  $X_c = R$  and can be calculated using the formula below:

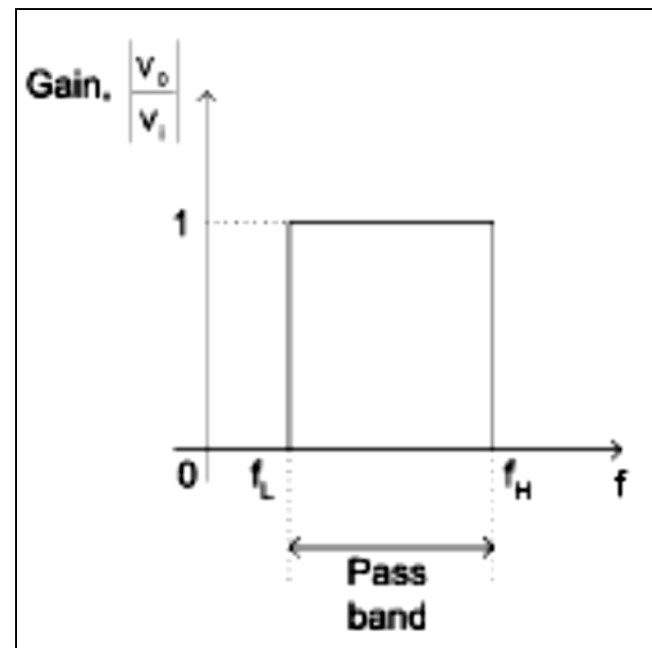
$$f_c = \frac{1}{2\pi RC}$$

# Band-Pass Filter Response

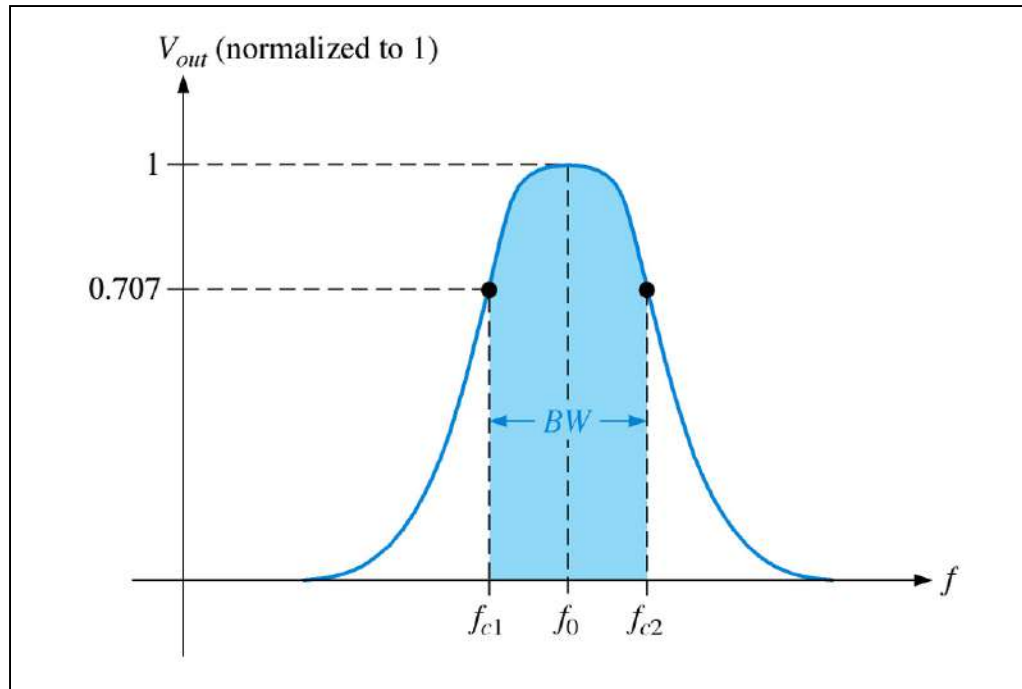
- A **band-pass filter** passes all signals lying within a band between a **lower-frequency limit** and **upper-frequency limit** and essentially rejects all other frequencies that are outside this specified band.



Actual response



Ideal response



➤ The **bandwidth (BW)** is defined as the **difference** between the **upper critical frequency ( $f_{c2}$ )** and the **lower critical frequency ( $f_{c1}$ )**.

$$BW = f_{c2} - f_{c1}$$

➤ The frequency about which the pass band is centered is called the ***center frequency,  $f_o$***  and defined as the geometric mean of the critical frequencies.

$$f_o = \sqrt{f_{c1} f_{c2}}$$

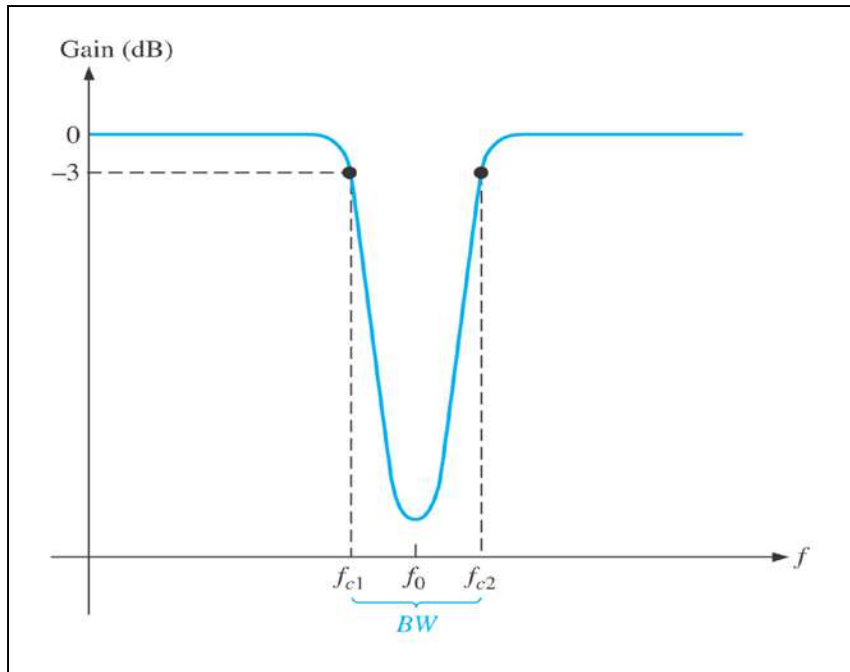
- The **quality factor ( $Q$ )** of a band-pass filter is the ratio of the center frequency to the bandwidth.

$$Q = \frac{f_o}{BW}$$

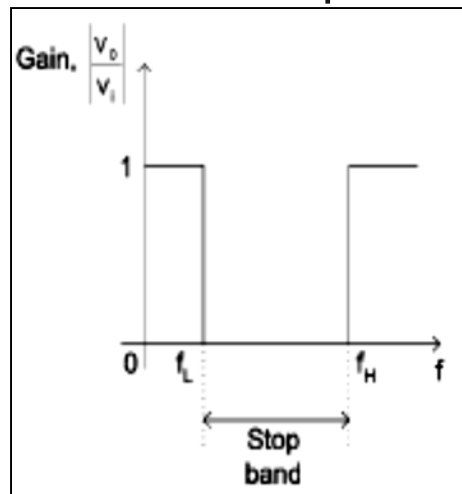
- The higher value of  $Q$ , the narrower the bandwidth and the better the selectivity for a given value of  $f_o$ .
- ( $Q > 10$ ) as a narrow-band or ( $Q < 10$ ) as a wide-band
- The quality factor ( $Q$ ) can also be expressed in terms of the damping factor ( $DF$ ) of the filter as :

$$Q = \frac{1}{DF}$$

# Band-Stop Filter Response



Actual response



Ideal response

➤ **Band-stop filter** is a filter which its operation is **opposite** to that of the band-pass filter because the frequencies **within** the bandwidth are **rejected**, and the frequencies above  $f_{c1}$  and  $f_{c2}$  are **passed**.

➤ For the band-stop filter, the **bandwidth** is a band of frequencies between the 3 dB points, just as in the case of the band-pass filter response.



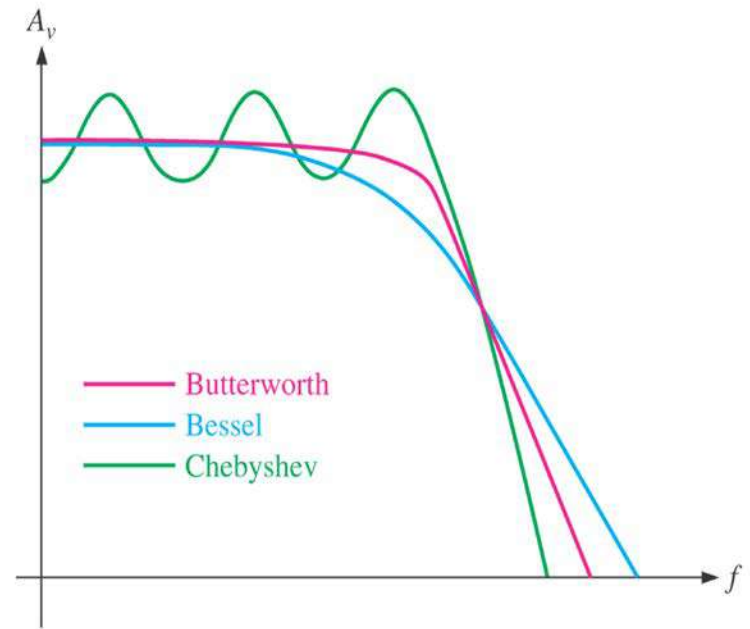
# FILTER RESPONSE CHARACTERISTICS

➤ There are **3** characteristics of filter response :

i) **Butterworth** characteristic

ii) **Chebyshev** characteristic

iii) **Bessel** characteristic.

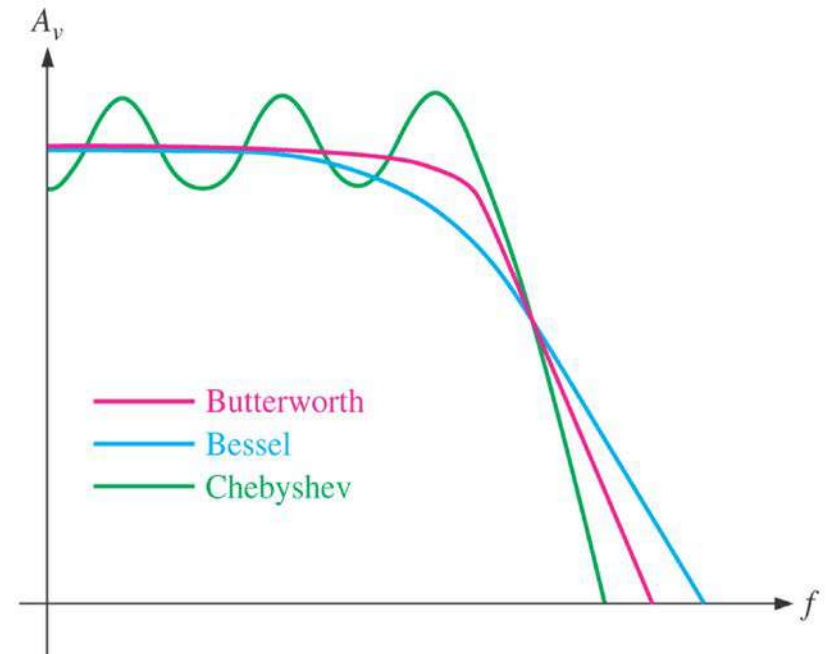


Comparative plots of three types of filter response characteristics.

➤ Each of the characteristics is identified by the **shape of the response curve**

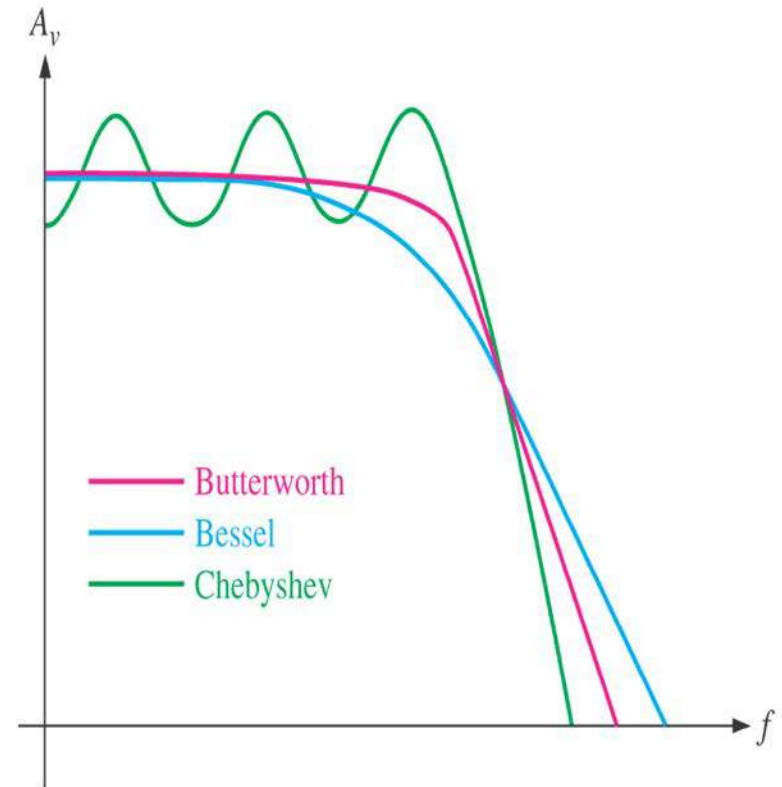
# Butterworth Characteristic

- Filter response is characterized by **flat amplitude response** in the passband.
- Provides a roll-off rate of -20 dB/decade/pole.
- Filters with the Butterworth response are normally used when all frequencies in the passband must have the **same gain**.



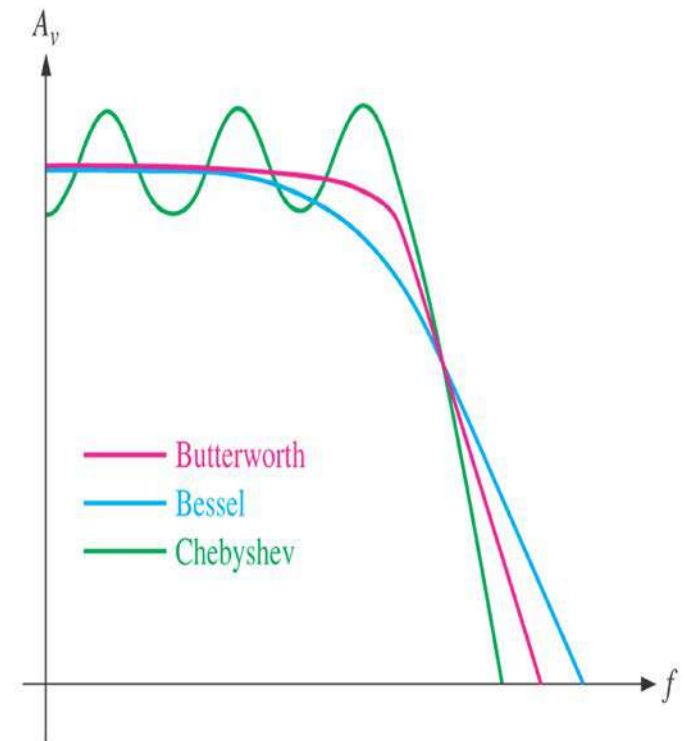
# Chebyshev Characteristic

- Filter response is characterized by **overshoot** or **ripples** in the passband.
- Provides a roll-off rate greater than -20 dB/decade/pole.
- Filters with the Chebyshev response can be implemented with **fewer poles** and **less complex circuitry** for a given roll-off rate



# Bessel Characteristic

- Filter response is characterized by a **linear characteristic**, meaning that the phase shift increases linearly with frequency.
- Filters with the Bessel response are used for filtering pulse waveforms without distorting the shape of waveform.



# DAMPING FACTOR

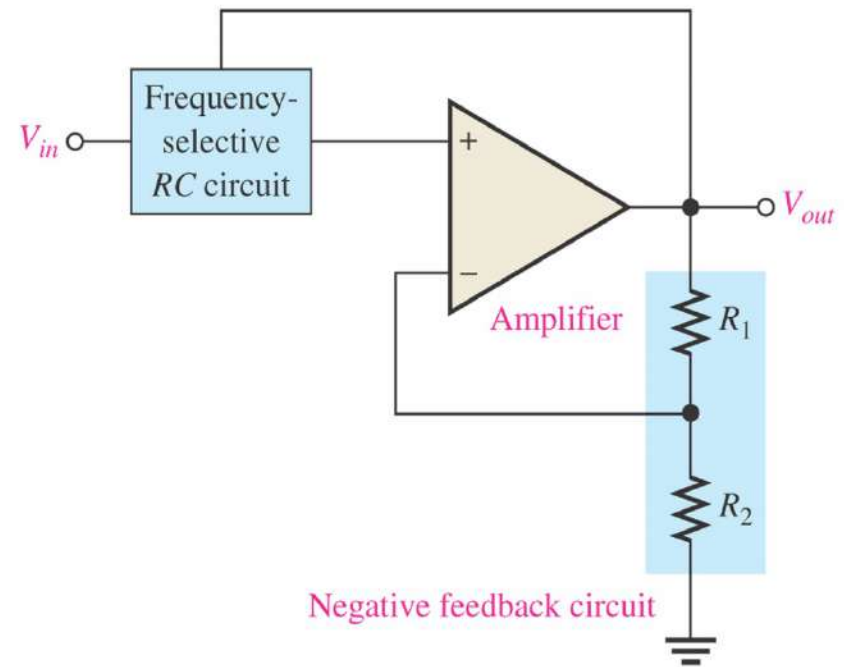
➤ The **damping factor (DF)** of an active filter determines which response characteristic the filter exhibits.

➤ This active filter consists of **an amplifier, a negative feedback circuit** and **RC circuit**.

➤ The amplifier and feedback are connected in a **non-inverting configuration**.

➤ DF is determined by the negative feedback and defined as :

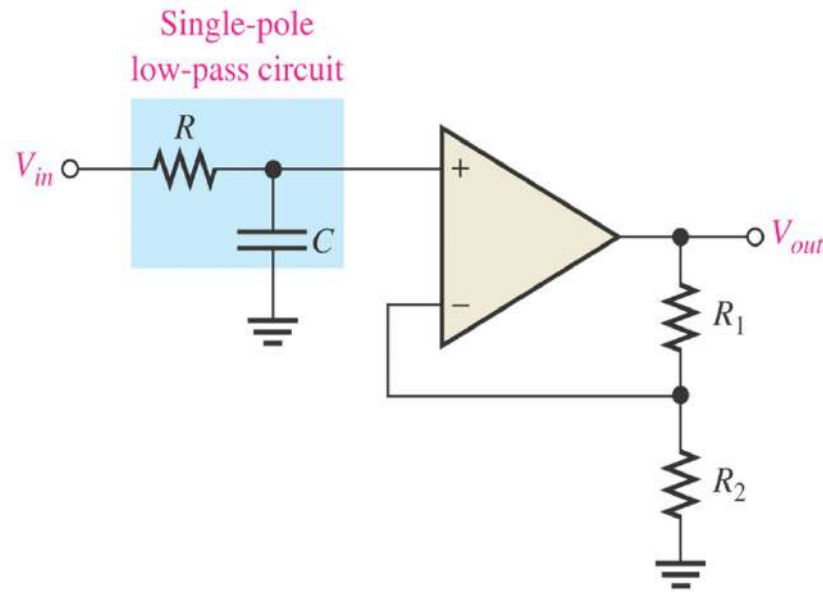
$$DF = 2 - \frac{R_1}{R_2}$$



General diagram of active filter

- The value of DF required to produce a desired response characteristics depends on **order** (number of poles) of the filter.
- A pole (single pole) is simply **one resistor** and **one capacitor**.
- The **more poles** filter has, the faster its roll-off rate

# CRITICAL FREQUENCY AND ROLL-OFF RATE



One-pole (first-order) low-pass filter.

- The **critical frequency,  $f_c$**  is determined by the values of **R** and **C** in the frequency-selective RC circuit.
- Each **RC** set of filter components represents a **pole**.
- **Greater roll-off rates** can be achieved with **more poles**.
- Each pole represents a **-20dB/decade** increase in roll-off.

- For a single-pole (first-order) filter, the critical frequency is :

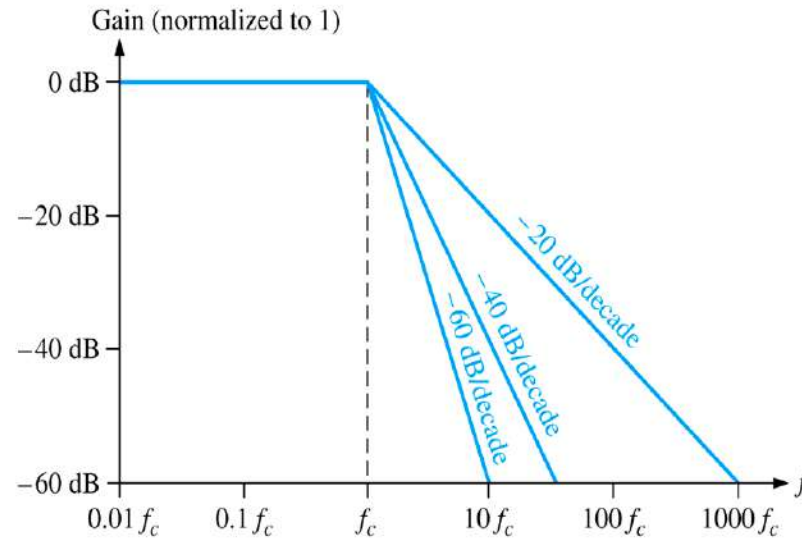
$$f_c = \frac{1}{2\pi RC}$$

- The above formula can be used for both low-pass and high-pass filters.

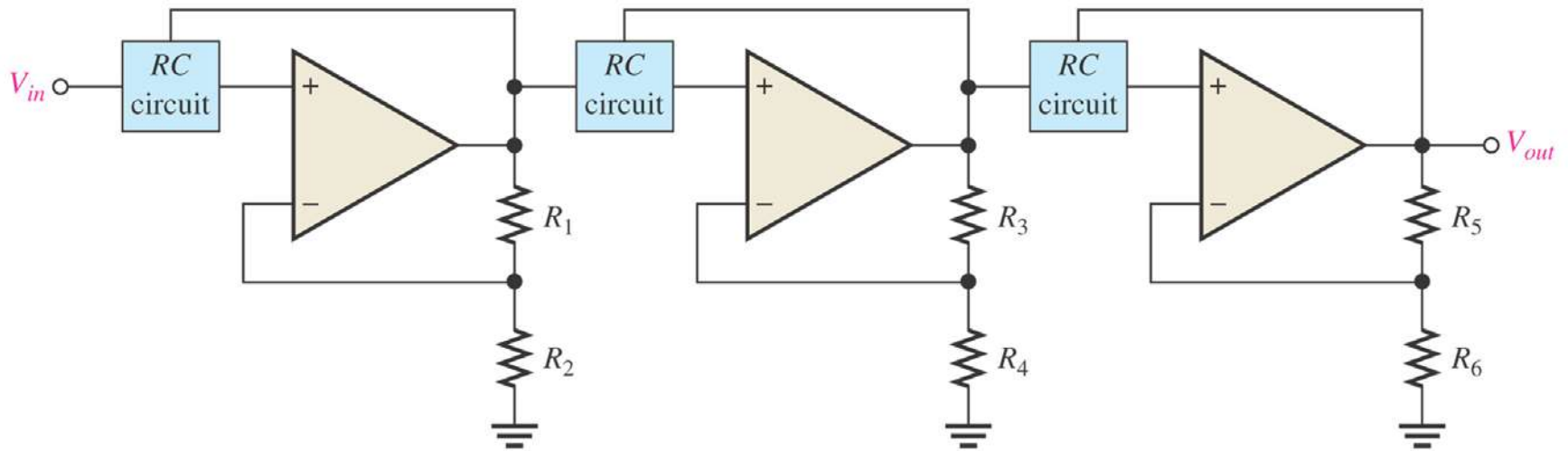


➤ The number of poles determines the roll-off rate of the filter. For example, a Butterworth response produces  $-20\text{dB/decade/pole}$ . This means that:

- **One-pole (first-order)** filter has a roll-off of  $-20\text{ dB/decade}$
- **Two-pole (second-order)** filter has a roll-off of  $-40\text{ dB/decade}$
- **Three-pole (third-order)** filter has a roll-off of  $-60\text{ dB/decade}$



➤ The number of filter poles can be increased by ***cascading***. To obtain a filter with three poles, cascade a two-pole with one-pole filters.



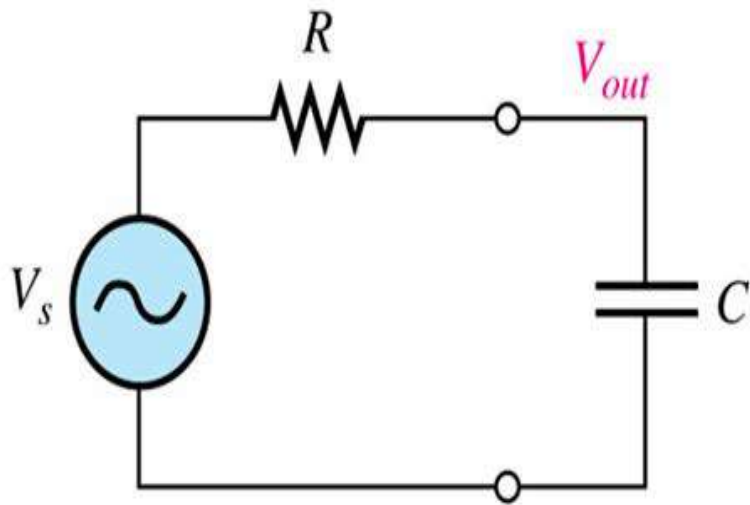
Three-pole (third-order) low-pass filter.

# ACTIVE LOW-PASS FILTERS

Advantages of active filters over passive filters (R, L, and C elements only):

1. By containing the op-amp, active filters can be designed to provide required gain, and hence **no signal attenuation** as the signal passes through the filter.
2. **No loading problem**, due to the high input impedance of the op-amp prevents excessive loading of the driving source, and the low output impedance of the op-amp prevents the filter from being affected by the load that it is driving.
3. **Easy to adjust over a wide frequency range** without altering the desired response.

➤ Figure below shows the basic Low-Pass filter circuit



(b) Basic low-pass circuit

At critical frequency,

Resistance = Capacitance

$$R = X_c$$

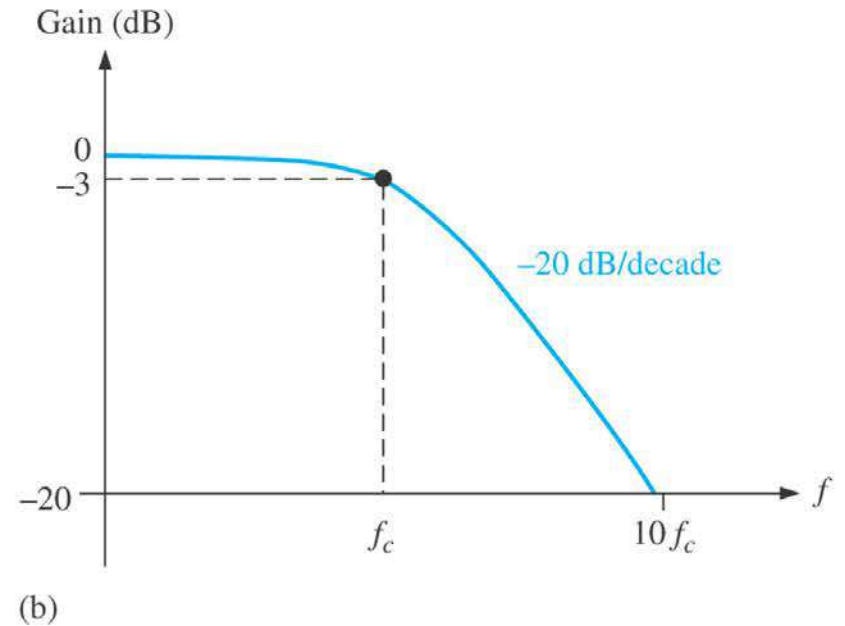
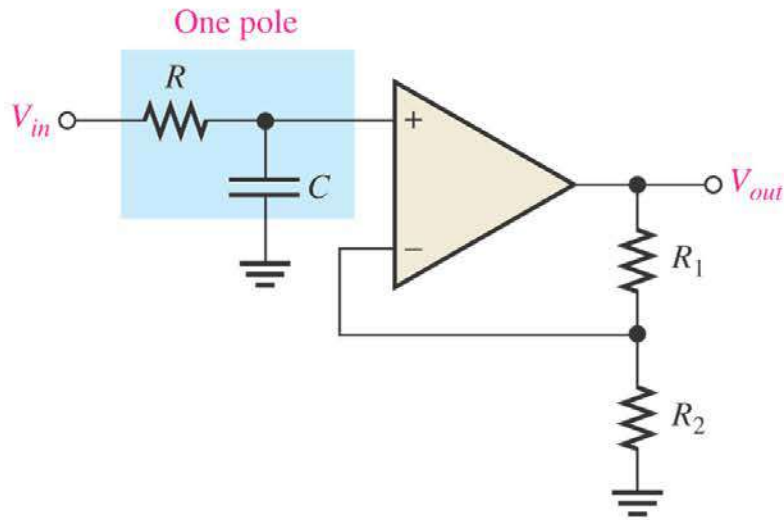
$$R = \frac{1}{\omega_c C}$$

$$R = \frac{1}{2\pi f_c C}$$

So, critical frequency ;

$$f_c = \frac{1}{2\pi RC}$$

# Single-Pole Filter



Single-pole active low-pass filter and response curve.

- This filter provides a roll-off rate of -20 dB/decade above the critical frequency.

➤ The op-amp in single-pole filter is connected as a noninverting amplifier with the closed-loop voltage gain in the passband is set by the values of  $R_1$  and  $R_2$  :

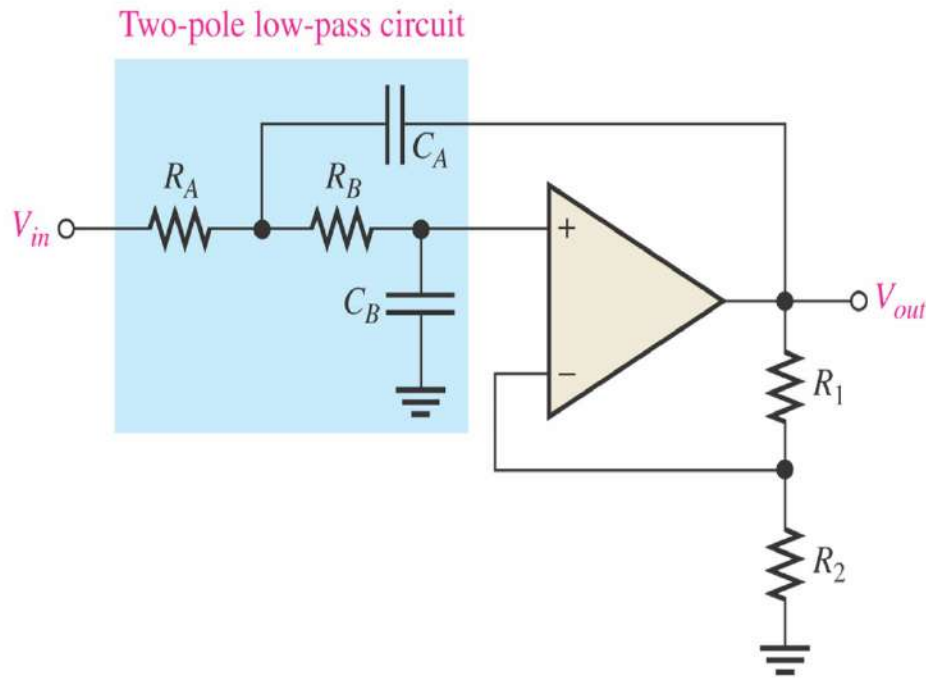
$$A_{cl(NI)} = \frac{R_1}{R_2} + 1$$

➤ The critical frequency of the single-pole filter is :

$$f_c = \frac{1}{2\pi RC}$$

# Sallen-Key Low-Pass Filter

- **Sallen-Key** is one of the most common configurations for a **second order** (two-pole) filter.



- There are two low-pass RC circuits that provide a **roll-off of -40 dB/decade above  $f_c$**  (assuming a Butterworth characteristics).
- One RC circuit consists of  $R_A$  and  $C_A$ , and the second circuit consists of  $R_B$  and  $C_B$ .

Basic Sallen-Key low-pass filter.

➤ The critical frequency for the Sallen-Key filter is :

$$f_c = \frac{1}{2\pi\sqrt{R_A R_B C_A C_B}}$$

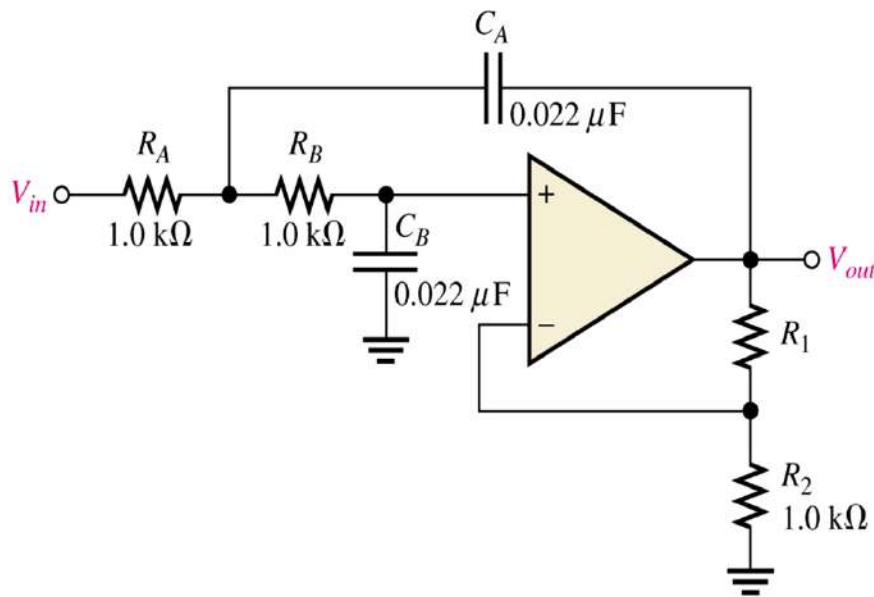
➤ For  $R_A = R_B = R$  and  $C_A = C_B = C$ , thus the critical frequency :

$$f_c = \frac{1}{2\pi RC}$$



# Example :

- Determine critical frequency
- Set the value of  $R_1$  for Butterworth response by giving that Butterworth response for second order is 0.586



- Critical frequency

$$f_c = \frac{1}{2\pi RC} = 7.23 \text{ kHz}$$

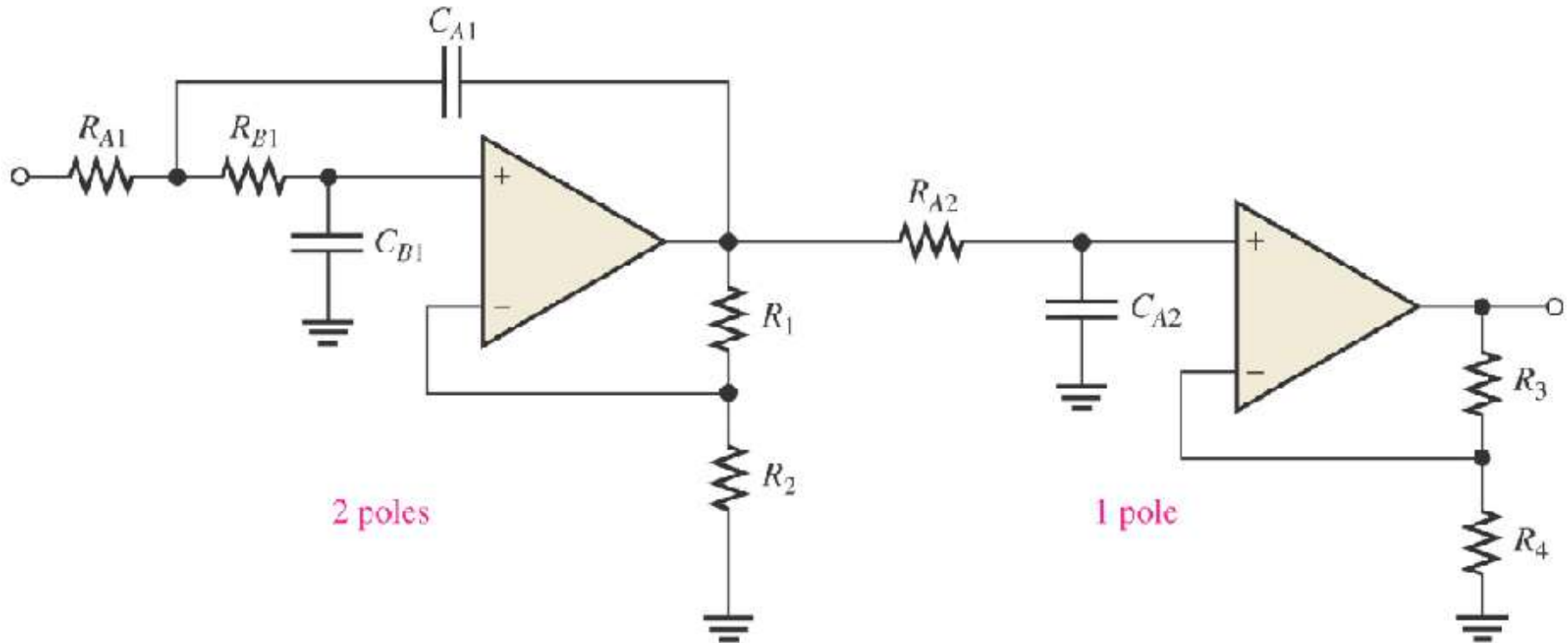
- Butterworth response given  $R_1/R_2 = 0.586$

$$R_1 = 0.586 R_2$$

$$R_1 = 586 \text{ k}\Omega$$

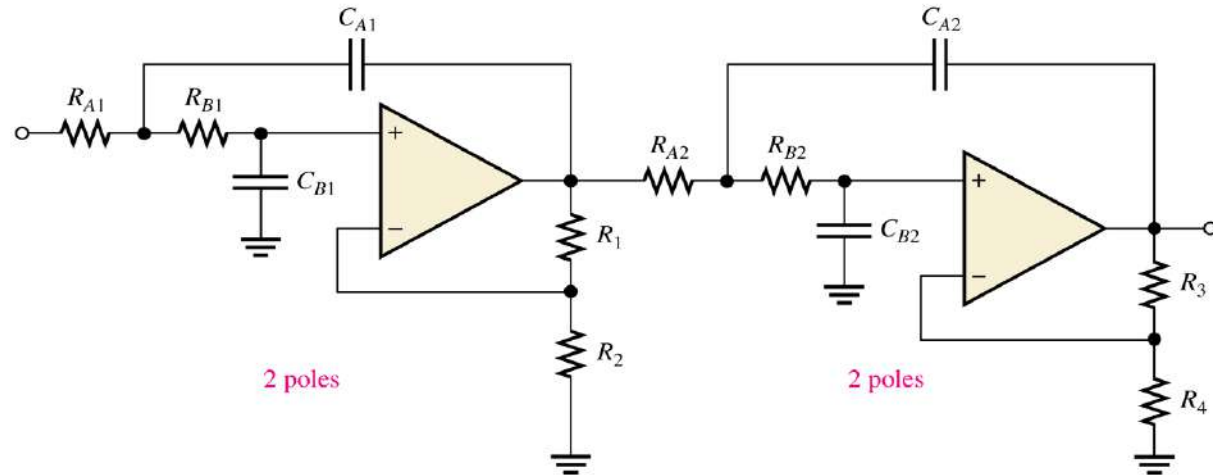
# Cascading Low-Pass Filter

- A **three-pole filter** is required to provide a roll-off rate of **-60 dB/decade**. This is done by cascading a **two-pole Sallen-Key low-pass filter** and a **single-pole low-pass filter**.



Cascaded low-pass filter: third-order configuration.

➤ A **four-pole filter** is required to provide a roll-off rate of **-80 dB/decade**. This is done by cascading a **two-pole Sallen-Key low-pass filter** and a **two-pole Sallen-Key low-pass filter**.

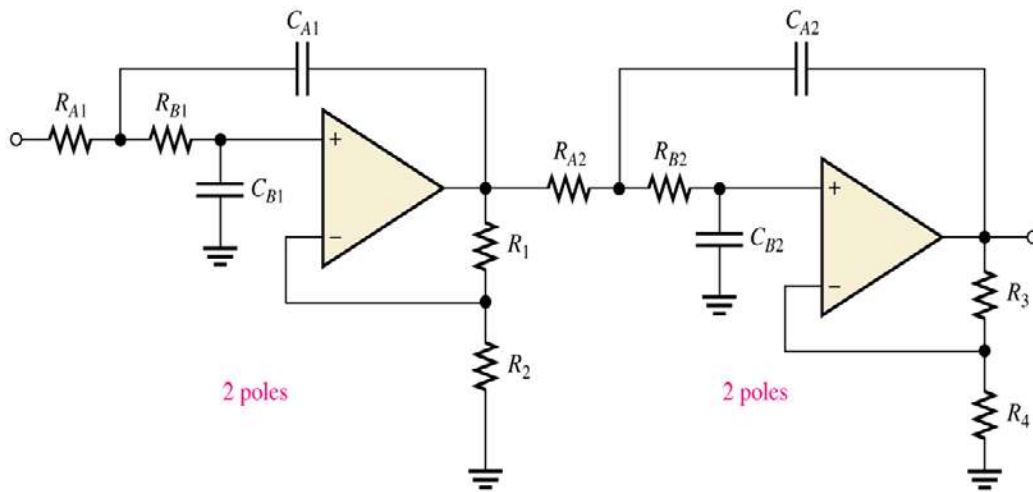


(b) Fourth-order configuration

Cascaded low-pass filter: fourth-order configuration.

# Example :

- Determine the capacitance values required to produce a critical frequency of 2680 Hz if all resistors in RC low pass circuit is 1.8k $\Omega$



(b) Fourth-order configuration

$$f_c = \frac{1}{2\pi RC}$$

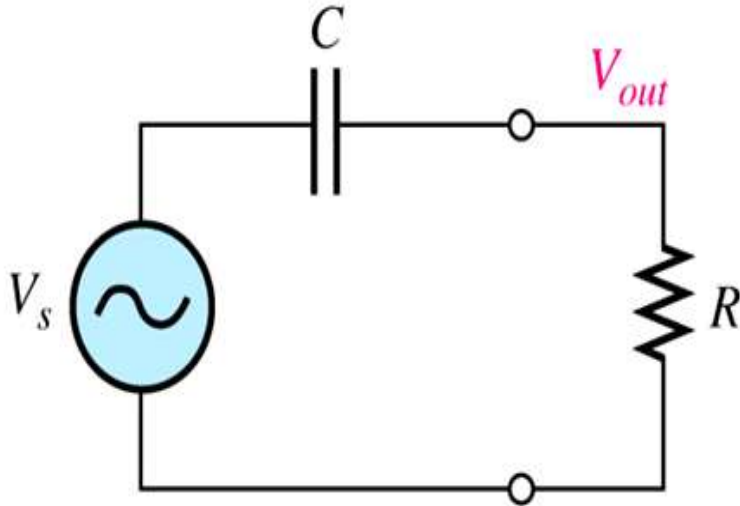
$$C = \frac{1}{2\pi f_c R} = 0.033 \mu F$$

$$C_{A1} = C_{B1} = C_{A2} = C_{B2} = 0.033 \mu f$$

- Both stages must have the same  $f_c$ . Assume equal-value of capacitor

# ACTIVE HIGH-PASS FILTERS

➤ Figure below shows the basic High-Pass filter circuit :



(b) Basic high-pass circuit

At critical frequency,

Resistance = Capacitance

$$R = X_c$$

$$R = \frac{1}{\omega_c C}$$

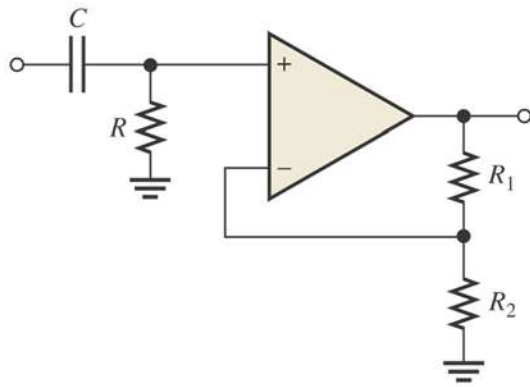
$$R = \frac{1}{2\pi f_c C}$$

So, critical frequency ;

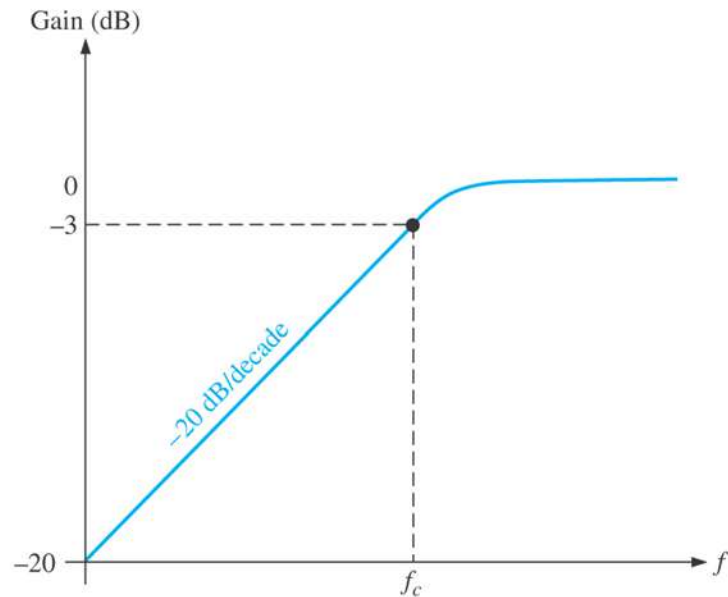
$$f_c = \frac{1}{2\pi RC}$$

# Single-Pole Filter

- In high-pass filters, the roles of the **capacitor** and **resistor** are **reversed** in the RC circuits as shown from Figure (a). The negative feedback circuit is the same as for the low-pass filters.
- Figure (b) shows a high-pass active filter with a  $-20\text{dB/decade}$  roll-off



(a)



(b)

Single-pole active high-pass filter and response curve.

➤ The op-amp in single-pole filter is connected as a noninverting amplifier with the closed-loop voltage gain in the passband is set by the values of  $R_1$  and  $R_2$  :

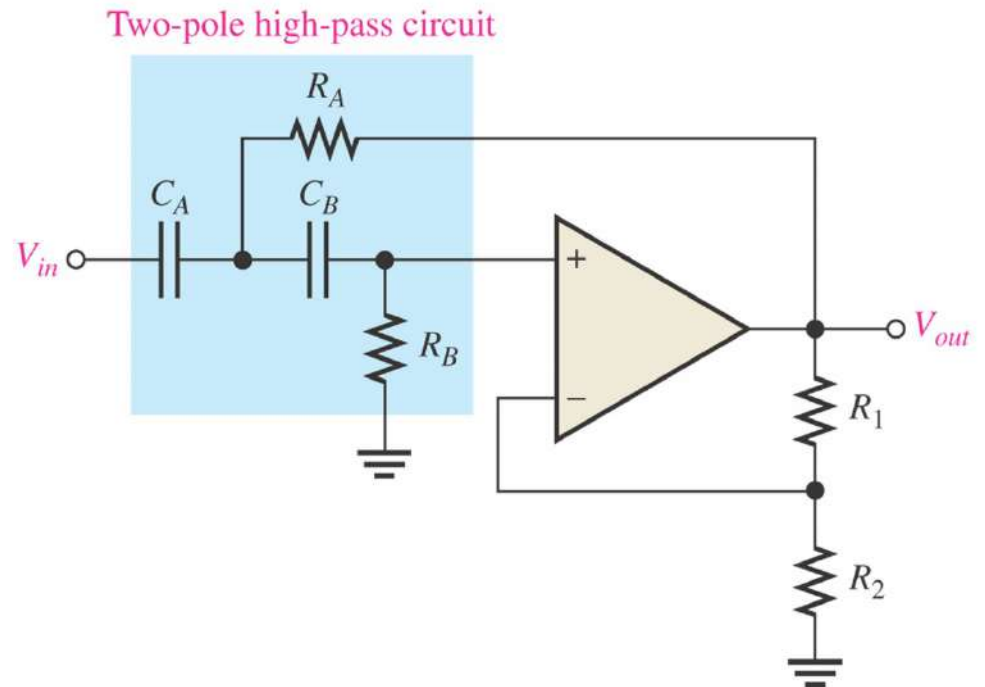
$$A_{cl(NI)} = \frac{R_1}{R_2} + 1$$

➤ The critical frequency of the single-pole filter is :

$$f_c = \frac{1}{2\pi RC}$$

# Sallen-Key High-Pass Filter

- Components  $R_A$ ,  $C_A$ ,  $R_B$ , and  $C_B$  form the **second order** (two-pole) frequency-selective circuit.
- The position of the resistors and capacitors in the frequency-selective circuit are **opposite** in low pass configuration.
- There are two high-pass RC circuits that provide a **roll-off of -40 dB/decade above  $f_c$**
- The **response characteristics** can be optimized by proper selection of the **feedback resistors**,  $R_1$  and  $R_2$ .



Basic Sallen-Key high-pass filter.



➤ The critical frequency for the Sallen-Key filter is :

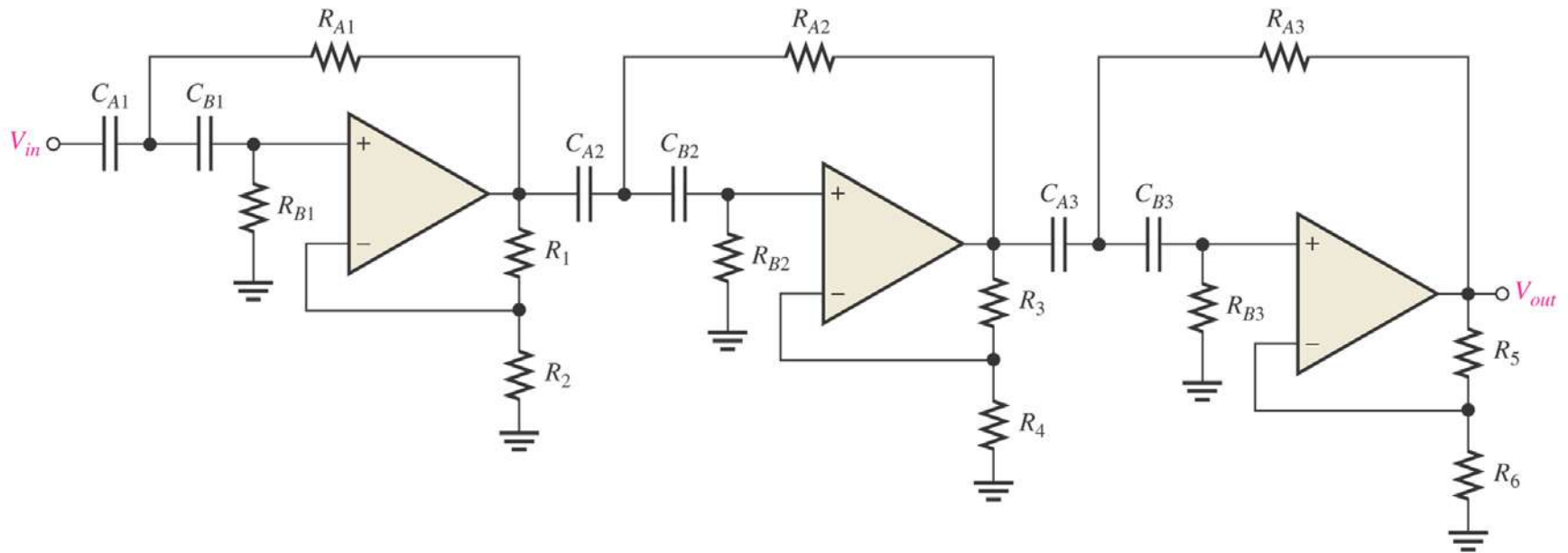
$$f_c = \frac{1}{2\pi\sqrt{R_A R_B C_A C_B}}$$

➤ For  $R_A = R_B = R$  and  $C_A = C_B = C$ , thus the critical frequency :

$$f_c = \frac{1}{2\pi RC}$$

# Cascading High-Pass Filter

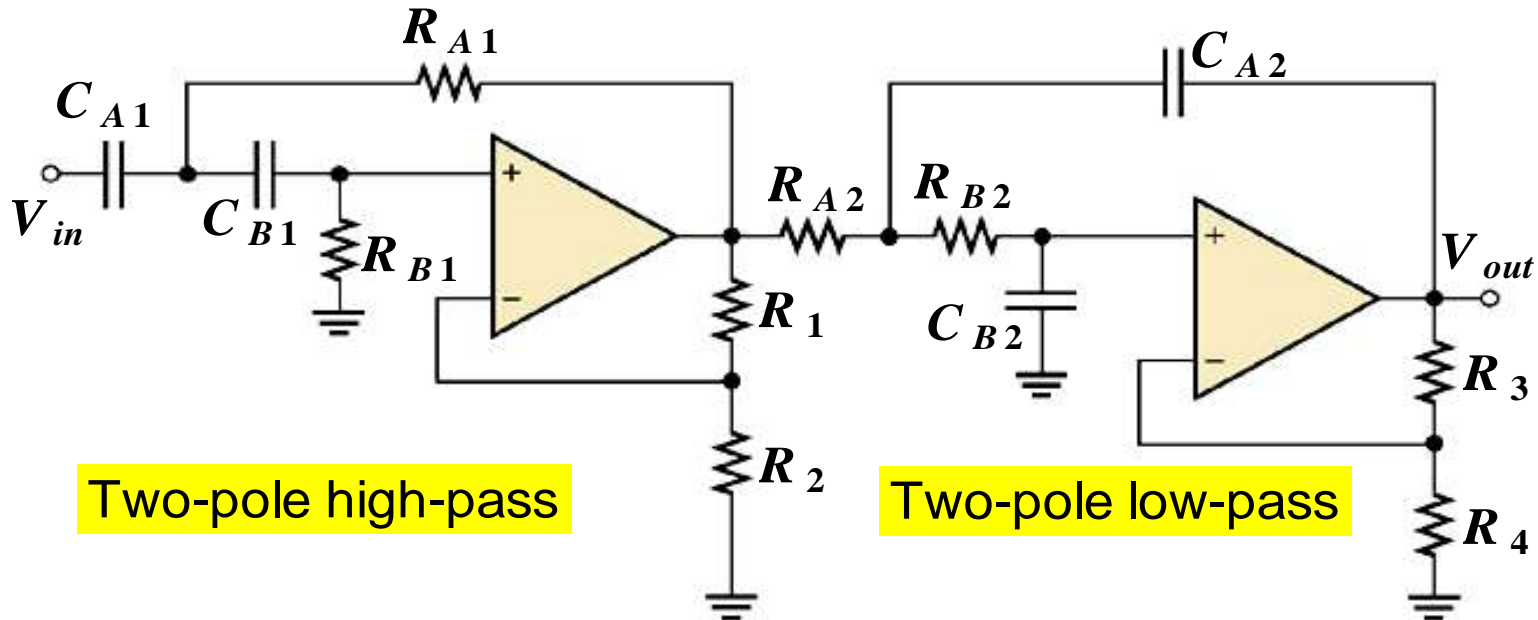
- As with the low-pass filter, first- and second-order high-pass filters can be cascaded to provide three or more poles and thereby create faster roll-off rates.
- A **six-pole high-pass filter** consisting of **three Sallen-Key two-pole** stages with the roll-off rate of **-120 dB/decade**.



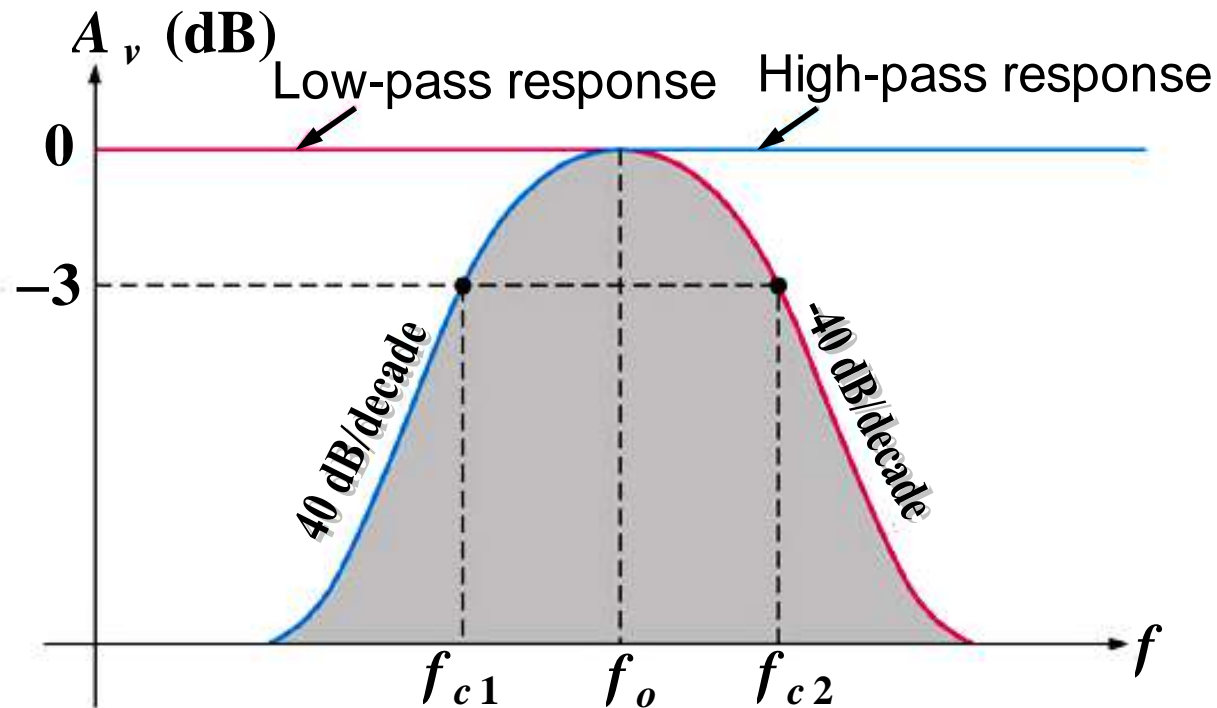
Sixth-order high-pass filter

# ACTIVE BAND-PASS FILTERS

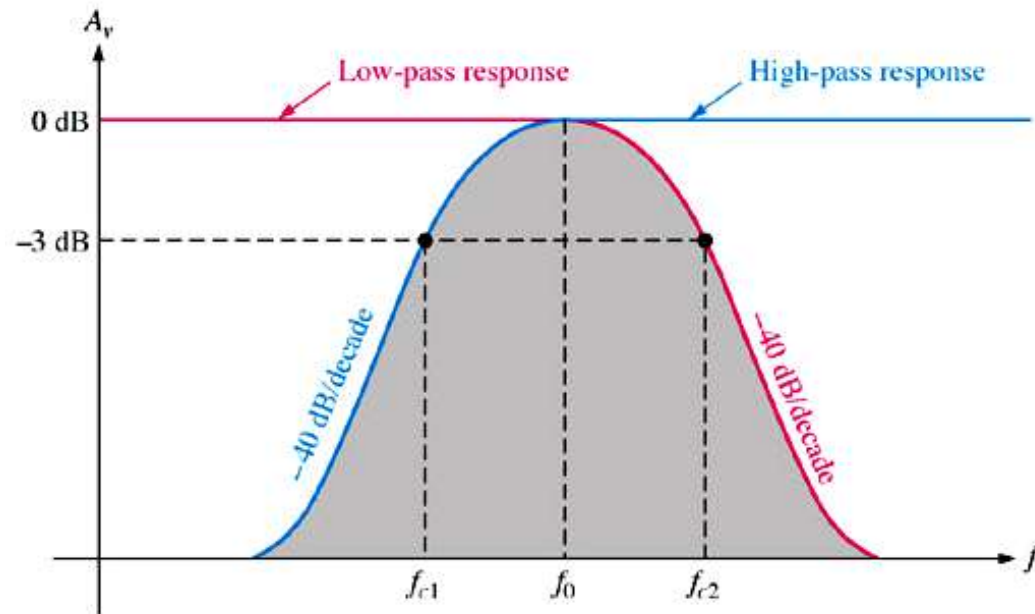
## Cascaded Low-Pass and High-Pass Filters



- Band-pass filter is formed by cascading a two-pole high-pass and two pole low-pass filter.
- Each of the filters shown is Sallen-Key Butterworth configuration, so that the roll-off rate are  $-40\text{dB/decade}$ .



- The lower frequency  $f_{c1}$  of the passband is the critical frequency of the high-pass filter.
- The upper frequency  $f_{c2}$  of the passband is the critical frequency of the low-pass filter.



➤ The following formulas express the three frequencies of the band-pass filter.

$$f_{c1} = \frac{1}{2\pi\sqrt{R_{A1}R_{B1}C_{A1}C_{B1}}}$$

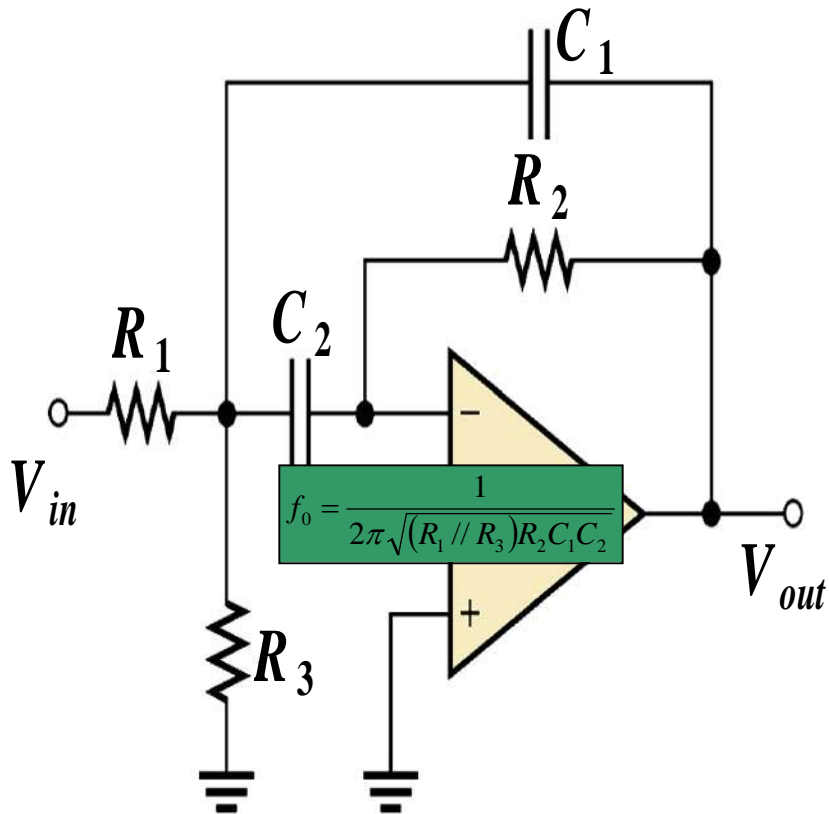
$$f_{c2} = \frac{1}{2\pi\sqrt{R_{A2}R_{B2}C_{A2}C_{B2}}}$$

$$f_0 = \sqrt{f_{c1}f_{c2}}$$

➤ If equal-value components are used in implementing each filter,

$$f_c = \frac{1}{2\pi RC}$$

# Multiple-Feedback Band-Pass Filter



- The low-pass circuit consists of  $R_1$  and  $C_1$ .
- The high-pass circuit consists of  $R_2$  and  $C_2$ .
- The feedback paths are through  $C_1$  and  $R_2$ .
- Center frequency;

- By making  $C_1 = C_2 = C$ , yields

$$f_0 = \frac{1}{2\pi C} \sqrt{\frac{R_1 + R_3}{R_1 R_2 R_3}}$$

- The resistor values can be found by using following formula

$$R_1 = \frac{Q}{2\pi f_0 C A_o}$$

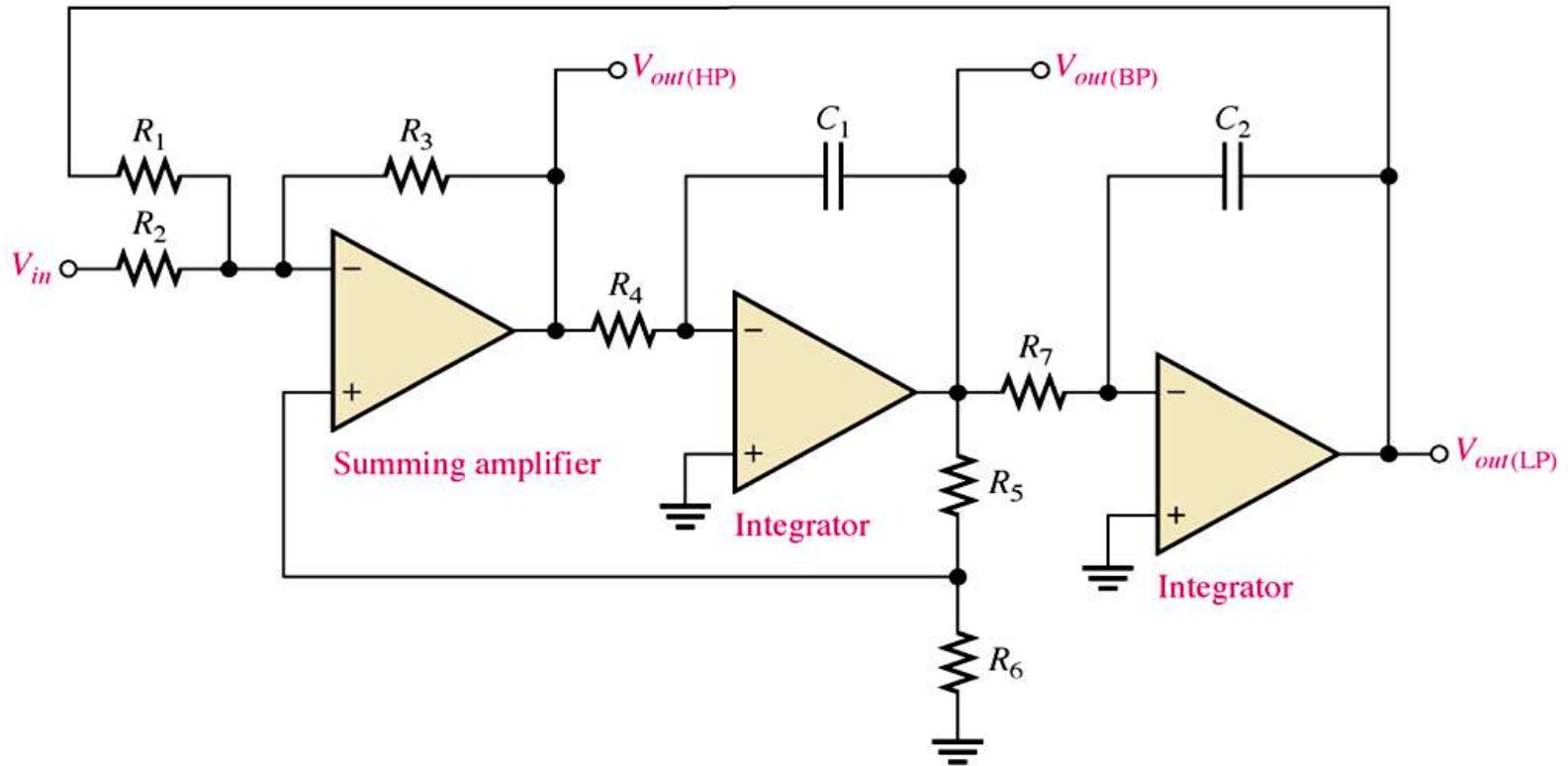
$$R_2 = \frac{Q}{\pi f_0 C}$$

$$R_3 = \frac{Q}{2\pi f_0 C (2Q^2 - A_o)}$$

- The maximum gain,  $A_o$  occurs at the center frequency.

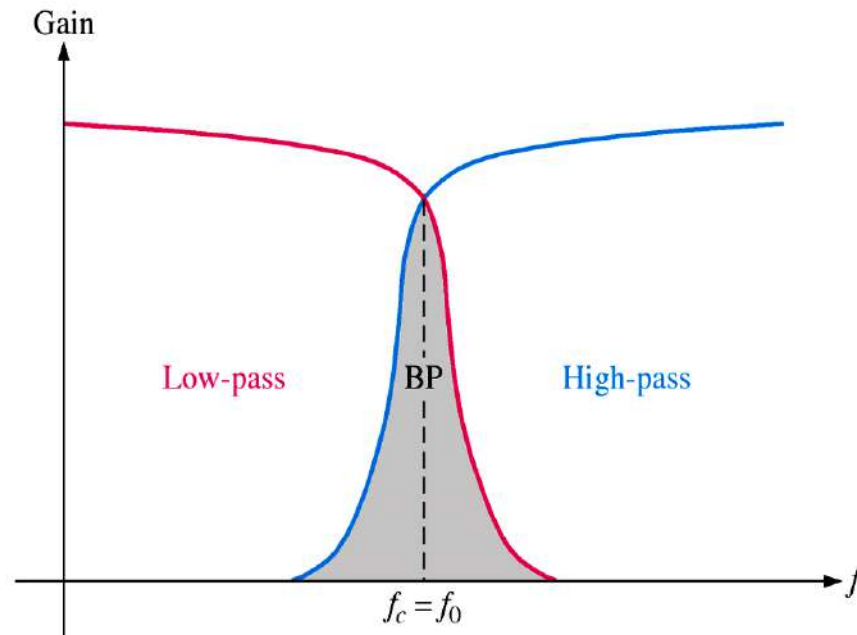
# State-Variable Filter

- State-Variable BPF is widely used for band-pass applications.





- It consists of a summing amplifier and two integrators.
- It has outputs for low-pass, high-pass, and band-pass.
- The center frequency is set by the integrator RC circuits.
- The critical frequency of the integrators usually made equal
- $R_5$  and  $R_6$  set the  $Q$  (bandwidth).



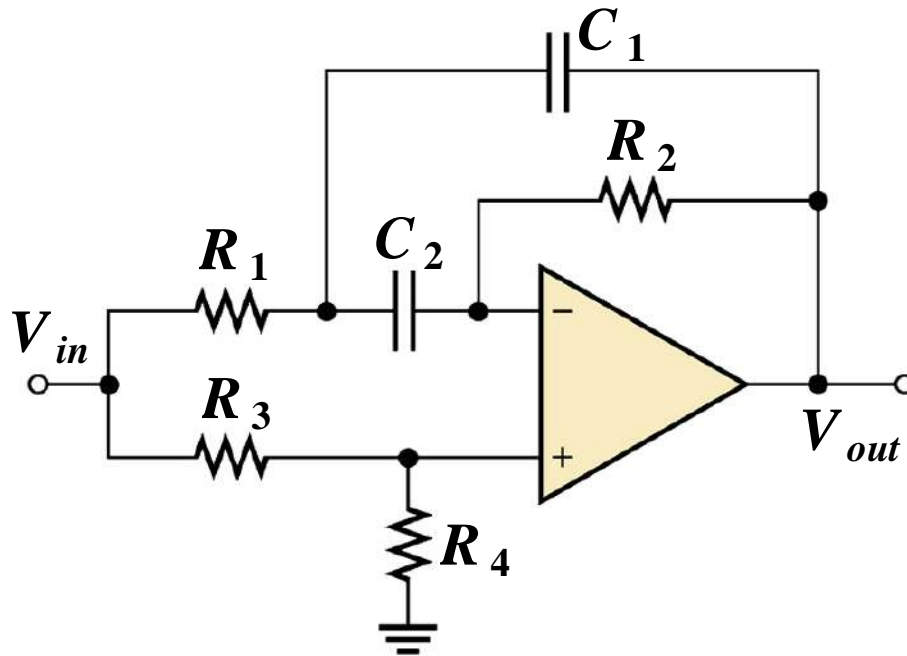
- The band-pass output peaks sharply the center frequency giving it a high  $Q$ .

➤ The Q is set by the feedback resistors  $R_5$  and  $R_6$  according to the following equations :

$$Q = \frac{1}{3} \left( \frac{R_5}{R_6} + 1 \right)$$

# ACTIVE BAND-STOP FILTERS

## *Multiple-Feedback Band-Stop Filter*



- The configuration is similar to the band-pass version BUT  $R_3$  has been moved and  $R_4$  has been added.
- The BSF is opposite of BPF in that it blocks a specific band of frequencies

# FILTER RESPONSE MEASUREMENT

- Measuring frequency response can be performed with typical bench-type equipment.
- It is a process of setting and measuring frequencies both outside and inside the known cutoff points in predetermined steps.
- Use the output measurements to plot a graph.
- More accurate measurements can be performed with sweep generators along with an oscilloscope, a spectrum analyzer, or a scalar analyzer.

# SUMMARY

- The bandwidth of a low-pass filter is the same as the upper critical frequency.
- The bandwidth of a high-pass filter extends from the lower critical frequency up to the inherent limits of the circuit.
- The band-pass passes frequencies between the lower critical frequency and the upper critical frequency.

- A band-stop filter rejects frequencies within the upper critical frequency and upper critical frequency.
- The Butterworth filter response is very flat and has a roll-off rate of  $-20$  B
- The Chebyshev filter response has ripples and overshoot in the passband but can have roll-off rates greater than  $-20$  dB

- The Bessel response exhibits a linear phase characteristic, and filters with the Bessel response are better for filtering pulse waveforms.
- A filter pole consists of one RC circuit. Each pole doubles the roll-off rate.  
The  $Q$  of a filter indicates a band-pass filter's selectivity. The higher the  $Q$  the narrower the bandwidth.
- The damping factor determines the filter response characteristic.